

Test Well Completion Report Dry Valley Test Well No. 1 Washoe County, Nevada

October, 2004

Prepared for: Intermountain Water Supply, Ltd. Reno, NV

Prepared by: InterFlow Hydrology, Inc Truckee, CA

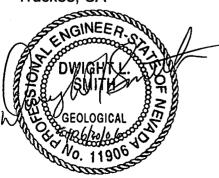


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Test Well Completion Report Dry Valley Test Well No. 1 Washoe County, Nevada

Introduction

In the summer of 2004, Intermountain Water Supply, Ltd completed a 6-inch diameter test well in Dry Valley, Washoe County, Nevada (Figure 1). The well is located in the NW ¼ SE ¼ Section 10, T24N, R28E, MDM, near the point of diversion for water rights Permit No. 66400. The purpose of Dry Valley Test Well No. 1 (DV-TW-1) is to collect ground water quality and aquifer data. This report presents a summary of hydrogeologic data collected during drilling and aquifer testing.

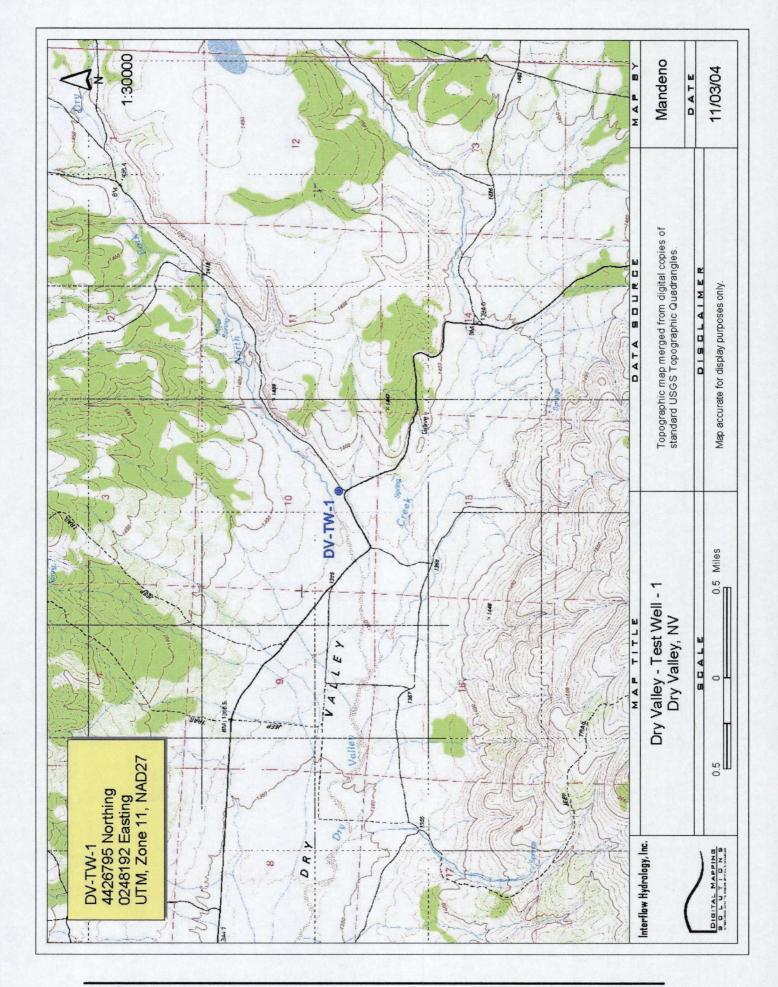
Summary

Well DV-TW-1 is constructed to 700 feet in depth and encountered two aquifer systems. The upper aquifer is unconfined and consists of interbedded gravel, sand and clay alluvium. Depth to ground water is only 5 feet below land surface and the aquifer extends to approximately 240 feet in depth. Near the base of this aquifer is a thin tuff (volcanic ash) unit at 224 feet in depth, marking the bottom of this aquifer as late Tertiary to early Quaternary (2 million years before present) basin-fill.

A deeper confined aquifer also exists from approximately 505 feet and to greater than 718 feet below land surface. This aquifer has a potentiometric head of 22 feet above land surface, resulting in approximately 35 gallons per minute (gpm) artesian flow from the well. The deep aquifer is in Tertiary basin-fill, with an apparent hydraulic conductivity lower than the upper aquifer. Separating the two aquifers is a sequence of basin-fill containing a greater amount of clay, and a thin interbedded basalt (volcanic flow) unit at 291 feet in depth.

Ground water chemistry at the test well is good, with all analyzed constituents meeting existing drinking water standards, including the forthcoming arsenic standard to be implemented in year 2006. Water produced from the test well is slightly geothermal, with temperatures measured between 75° and 85° F. The source of the geothermal water is the deep confined aquifer.

Two pumping tests were conducted at rates ranging from 100 to 305 gpm. The hydraulic efficiency of the 6-inch diameter test well is likely low (below 50%) due to construction materials and well diameter. A large-diameter (12 to 16-inch) higher-efficiency production well constructed at this location should be capable of producing at least 600 gpm. However, the calculated hydraulic conductivity of the test well is lower than expected for alluvium and poorly consolidated basin-fill, and water level recovery after the pumping tests was slow. It appears likely that a production well at this location will need to be operated with recovery (non-pumping) periods sufficient to sustain reasonable pumping water levels over the long-term.



Drilling and Well Construction

Drilling was accomplished using direct-circulation mud-rotary drilling methods by Humboldt Drilling and Pump Company, Winnemucca, Nevada. Drilling commenced on May 21, 2004 and the well was completed approximately two weeks thereafter. A 6-inch diameter pilot borehole was initially drilled to 718 feet in depth, with the cuttings geologically logged and an electric log performed on the borehole. The pilot borehole was then reamed to a 12-inch diameter borehole to accommodate construction of a 6-inch diameter test well.

DV-TW-1 well construction is as follows:

Material	<u>Depth Interval</u>
Blank casing (6-5/8 inch O.D., 0.188 wall thickness) Mill-slot perforated casing (3/16-inch quad-slotted) Blank casing Mill-slot perforated casing Blank casing with end cap Gravel pack (3/8-inch pea gravel) Cement Seal	Above land surface to 110 feet 110 to 240 feet 240 to 500 feet 500 to 700 feet 700 to 710 feet 100 to 720 feet Land surface to 100 feet

Problems (bridging) occurred during gravel pack installation, and the casing had to be removed by the driller and the 12-inch borehole re-drilled to remove gravel pack material and reset the casing. This has lead to some question as to potential borehole plugging (introduction of drilling mud into the borehole twice), which were later addressed by additional swabbing and air-lifting development.

Upon completion, the well had an artesian flow of approximately 35 gpm of mildly geothermal water (85°F). The well was capped and a pressure gage installed, which measured 9.1 psi (21 feet of head at the gage) in August 2004.

The driller's report for the test well is included in Appendix A.

Geologic Logging

Formation samples were collected at 10-foot depth intervals during pilot borehole drilling and logged by a hydrogeologist. Electric logging of the borehole was also conducted. Logs are included in Appendix A.

In summary, the geologic logging indicates two aquifers were encountered. An upper aquifer exists from near ground surface to approximately 240 feet in depth, and appears to be unconfined (perhaps semi-confined at depth). Static water level in the upper aquifer is approximately 5 feet below ground surface. Alluvium encountered is predominantly gravelly and clayey sand. Cleaner sands were logged from 0 to 35 feet, 65 to 85 feet, 150 to 170 feet, 195 to 224 feet, and 228 to 254 feet in depth. A thin tuff layer (volcanic ash) is present at approximately 224 feet in depth, which probably marks the late-Quaternary to early-Tertiary time-frame as interpreted from nearby geologic mapping and rock descriptions by Grose and others (2000) and Henry and others (2004). Electric logging suggests significant interbedded water-bearing strata throughout this upper aquifer (Appendix A).

A reddish-brown clay stratum is present from 261 to 291 feet in depth, and is underlain by a possible basalt layer (volcanic flow rock) from 291 to 300 feet in depth (could be a large boulder).

Lithology of Tertiary basin-fill between 300 to 505 feet is interbedded sands, gravels and clays, with significant clays at 335 to 361, 385 to 355, 425 to 455, and 495 to 505 feet in depth. Electric logging suggests this basin-fill is hydraulically tighter with minor water-bearing potential as compared to the overlying alluvium.

From 505 to 718 feet, significant sands were encountered, with interbedded clay strata at 540, 575, 600 to 610, 637 to 658, and 685 to 690 feet in depth. Dark brown clay at 637 to 658 feet in depth was unusually soft. These notably coarse-grained Tertiary basin-fill materials comprise a deeper confined aquifer. Geologic and electric logging suggests good water bearing properties in these deeper basin-fill deposits.

Water Chemistry Testing

General water chemistry was analyzed from two water samples collected from DV-TW-1. The first sample dated June 17, 2004 was collected at the end of initial well development by air-lifting methods. The second sample was collected on June 25, 2004 after approximately 23 hours of pumping at an average flow rate of 111 gpm.

All analyzed parameters meet current state and federal drinking water standards. The total dissolved solids content is excellent at 210 milligrams per liter (mg/L). Arsenic concentration is low at 0.005 mg/L, which meets the forthcoming year 2006 drinking water standard. Trace amounts of iron and manganese at 0.06 mg/L and 0.011 mg/L, respectively, are within drinking water standards.

Laboratory analytical reports are contained in Appendix B.

Aquifer Testing

Two aquifer tests were conducted on the test well. During both tests, water levels were recorded by both manual wire-line measurements and a water level transducer-recorder. Temperature data were also collected by the recorder which was installed in the well at a depth of approximately 200 feet. Miscellaneous conductivity measurements were taken during pumping with no noticeable changes observed. Water levels were monitored in a nearby stockwater pond built in the stream channel of the North Fork of Dry Valley Creek, with no changes observed during pumping.

The first test was commenced on June 24, 2004 at a pumping rate of approximately 300 gpm, and was reduced to a constant rate of approximately 100 gpm for the majority of the duration of the 24-hour test. Recovery water levels were measured following the pumping period (see Figure 2). This pumping test followed limited development of the test well via air-lifting. While produced water was noted to be clear during the end of air-lifting development, there was a concern that some aquifer plugging might have occurred during well construction, and a decision was made to more aggressively develop the well.

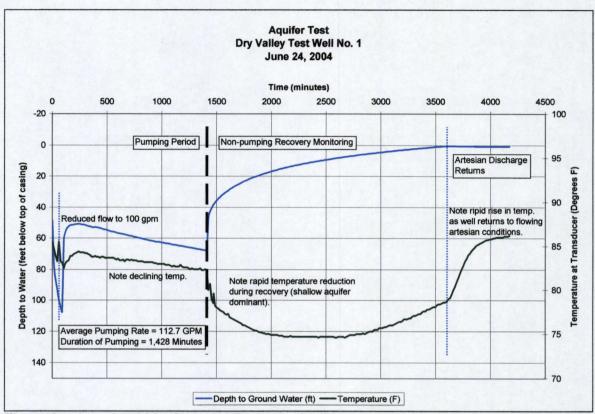


Figure 2 - June 24, 2004 Constant Rate Aguifer Test.

Following two days of additional swabbing and airlifting development, a step-drawdown test was conducted on August 16, 2004 for a pumping duration of 8.3 hours (see Figure 3). Pumping rates ranged from approximately 111 to 305 gpm (Figure 4), and some gains in production capacity were noted over the previous pumping test (approximately 30%). Recovery water levels were measured following the pumping period. An important observation is that the specific capacity of the test well (production per unit drawdown) increased with increasing flow rates (Figure 4). This is not normal, with an expected lowering of specific capacity with increasing flow rates, as a result of increased entrance velocity head losses (Driscoll, 1986). This tends to indicate that the test well is not completely developed, i.e., some formation damage (aquifer plugging) by drilling mud (bentonite) may be present.

Analyses of aquifer tests was performed using spreadsheet techniques published by Halford and Kuniansky (2002), and indicate an aquifer hydraulic conductivity of approximately 0.2 ft/day (ft/day = cubic feet per day per square foot of aquifer) (see Appendix C). This is a notably low hydraulic conductivity for sand dominated alluvium and basin-fill materials. Todd (1980) reports a representative range for fine to medium sand of approximately 8 to 40 ft/day, and Freeze and Cherry (1979) present a range for silty sands of approximately 0.1 to 100 ft/day.

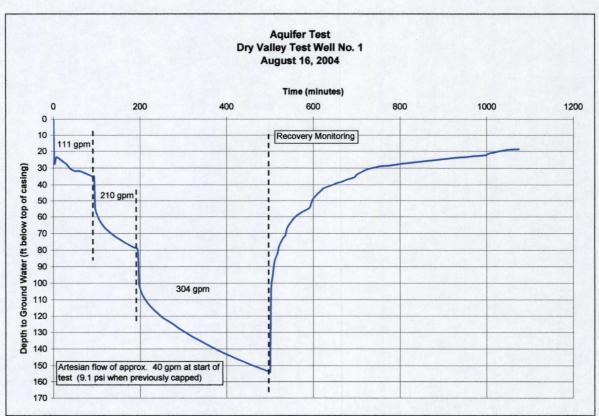


Figure 3 – August 16, 2004 Step Drawdown Aquifer Test.

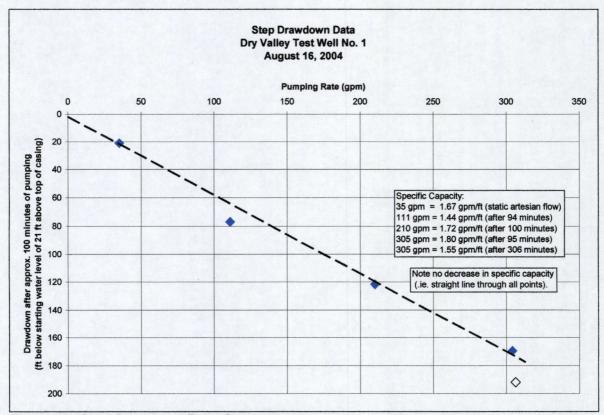


Figure 4 – Step Drawdown Data Summary.

Water temperature of artesian flow from DV-TW-1 is approximately 85°F. During pumping, the temperature of discharged water decreased. The trends in temperature changes during and after the pumping periods indicate that the deeper confined aquifer is the source of geothermal water and also the source of artesian flow produced from the well (Figure 2). The dominant aquifer contributing flow to the well during the aquifer tests appears to be the upper unconfined aquifer, also based on observations of temperature fluctuations and water-level recovery trends during and after pumping periods (Figure 2).

Recovery water-level monitoring following both aquifer tests suggests that the aquifer is slow to regain starting static water levels, although potential formation damage (drilling mud plugging problems) may be affecting the data. The observed time to return to starting static water level in the upper aquifer appears to the about 3 times the duration of pumping (Figure 5), and longer for the deeper confined aquifer. The duration of pumping tests were relatively short, and long-term monitoring of water levels will be necessary, should a production well be constructed at this location. The aquifer testing data suggest that production pumping at this location will need to be managed with recovery (non-pumping) periods in order to maintain long-term water levels at acceptable levels.

3× duration

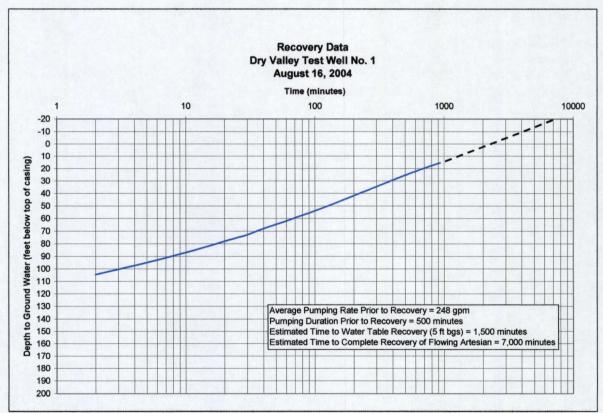
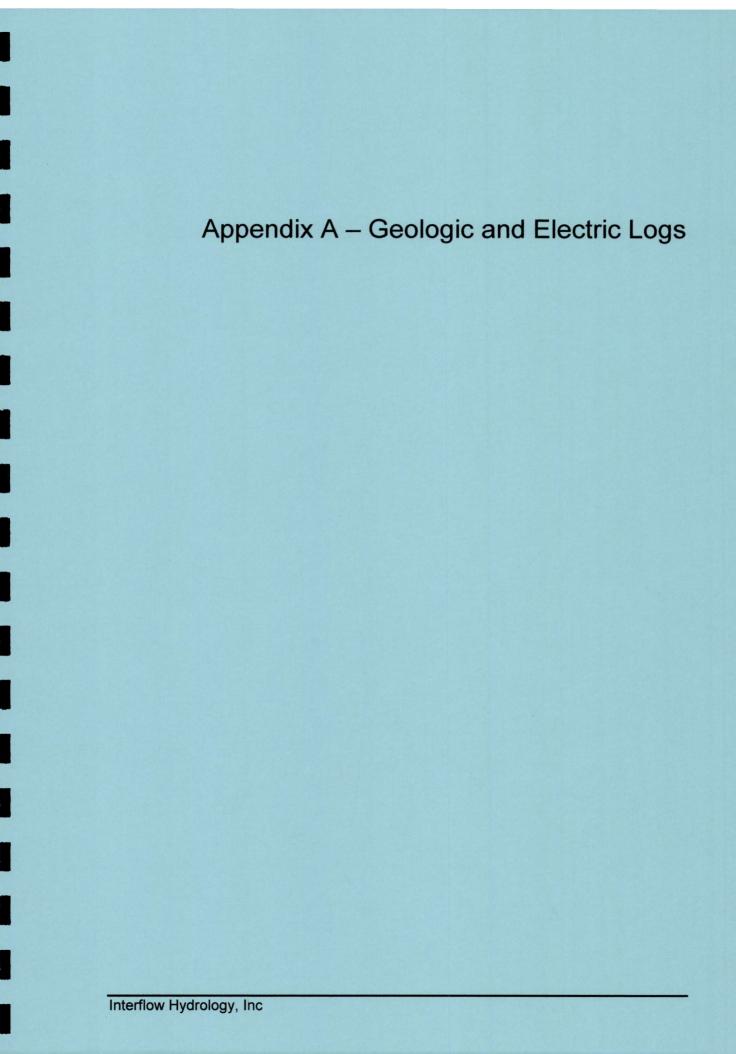


Figure 5 – Recovery Water Level Monitoring after August 16, 2004 Aquifer Test.

Well efficiency (a function of entrance velocity head losses in the well which create additional drawdown) is believed to be 50% or lower, based on the type of well construction materials (mill-slot perforated casing) and the relatively small diameter of the test well as compared to the pumped rates. A large-diameter production well constructed with continuous-slot well screen will likely yield at least 600 gpm. The duration of pumping at this type of rate would be dependent on monitoring and managing water-level drawdown in the well.

References

- Driscoll, F. G., 1986, Groundwater and Wells, Published by Johnson Division, St. Paul, Minnesota.
- Freeze, R. A, and Cherry, 1979, J. A., Groundwater, Published by Prentice-Hall, Inc., Englewood Cliffs, New Jersey.
- Grose, T.L.T., Mergner, M., Moar, R.R., Saucedo, G.J., and Little, J.D., 2000, Geologic Map of the Chilcoot 15' Quadrangle, Lassen and Plumas Counties, California, California Department of Conservation, Division of Mines and Geology, DMG Open-File Report 2000-23, 1 Plate, 1:62,500 scale.
- Halford, K. J., and Kuniansky, E. L., 2002, Documentation of Spreadsheets for the Analysis of Aquifer-Test and Slug-Test Data, US Geological Survey, Open-File Report 02-197.
- Henry, C. D., Faulds, J. E., dePolo, C. M., and Davis, D. A., 2004, Geology of the Dogskin Mountain Quadrangle, Northern Walker Lane, Nevada (including Preliminary Geologic Map, 1:24,000 scale), Nevada Bureau of Mines and Geology, Open-File Report 03-16.
- Todd, D. K., 1980, Groundwater Hydrology, Second Edition, Published by John Wiley & Sons, New York, New York.



DRY VALLEY TEST WELL NO. 1 (DV-TW-1)

Logged by: D. Smith
Drilling Commenced: May 21, 2004
Driller: Humboldt Drilling
Drilling Method: Mud Rotary (6-inch diameter borehole)

Page 1 of 3

Depth (ft)	Time	Lithology	Description
0	5-21-04 12:00		0 – 35: Brown Cobby Slighty Silty SAND, angular to subrounded predominantly volcanic derived (basalt).
20			25 45. Pro Crovelly Cl AVEV CAND w/set 200/ mad
40			35 – 45: Brn. Gravelly CLAYEY SAND, w/est. 30% med. plastic clay.
			45 – 55: Gravelly SAND, subangular to subrounded, minor clay stringers.
60			55 – 65: Gravelly CLAYEY SAND, 10-15% clay. 65 – 85: Brn. Gravelly Silty SAND.
80	13:15		85 – 90: Brown Gravelly Sandy CLAY.
100	13:35		90 – 101: Brn. Gravelly CLAYEY SAND, with est. 15% med. plastic clay (clay stringers). 101 – 104: Brown Gravelly Sandy CLAY.
120	14:10		104 – 120: Gravelly CLAYEY SAND, with est. 15% clay.
		-	120 – 135: Reddish Brn. Gravelly Sandy CLAY.135 – 150: Brn. Gravelly CLAYEY SAND, with est. 20% med.
140	14:30		plastic clay. 150 – 170: Brn. Slightly Clayey GRAVELLY SAND, subangular
160	14:50		to subrounded, gravel and coarse sand is predominantly basalt in med to fine grained lithic and quartz sand. 170 – 180: Brn. Gravelly CLAYEY SAND, with est. 20%.
180	15:05		180 – 195: Gravelly Sandy CLAY
200		-	195 – 224: Slightly Clayey GRAVELLY SAND, coarse grained, angular to subrounded sand particles, majority drk gray basalt, with yellow, white and pink feldspar, and clear quartz.
220	15:55		224 – 228: Lt. Reddish Gray TUFF (chips, micaeous, glassey). 228 – 254: Gray Slightly Clayey GRAVELLY SAND, same as
240			195 to 224 ft.
			254 – 257: Lt. Gray Sandy CLAY. 257 – 261: SAND, same as 228 – 254.

DRY VALLEY TEST WELL NO. 1 (DV-TW-1)

Logged by: D. Smith
Drilling Commenced: May 21, 2004
Driller: Humboldt Drilling
Drilling Method: Mud Rotary (6-inch diameter borehole)

Page 2 of 3

260	16:45	Jan 19 years	261 _ 201	Reddish Brn. Sandy CLAY.
200	, , , , ,		201-291.	Reduish Bill. Sandy CLAT.
280				
		PARTITION TO THE PARTITION OF THE PARTIT	291 – 300:	BASALT (cuttings are chips, hard – slow drilling).
300	5-22-04		300 – 315:	Gravelly CLAYEY SAND with est. 15% gray clay.
	9:45			
320				Slightly Clayey Gravelly SAND, angular to predominantly volcanic rock particles.
320			Subangulai	predominantly voicanic rock particles.
		The second secon		
340	10:20		335 – 361:	Sandy CLAY with est. 50% med. plastic clay.
340				
360	10:30			Brn. SAND, fine to coarse grained angular to I predominantly gray basalt particles with some
			feldspar and	
380	10:50			, , , , , , , , , , , , , , , , , , ,
			385 – 405:	Brn. CLAYEY GRAVELLY SAND w/est. 20% clay.
400	11:15			
400	11.15		405 425	Brn. CLAYEY SAND with occasional boulders
			(410).	DIT. OLIVIET GAND WITH OCCUSIONAL BOUNCERS
420	11:45			
			425 – 440:	Sandy CLAY with est. 50% low-med plastic clay.
440	12:10		440 – 450:	Brn. Clayey GRAVEL with est. 25% med plastic
440	12.10	0000	clay, subrou	unded gravel to 1/2-inch plus, dk. Gray volcanic.
				Sandy CLAY, 50% med plastic clay.
460		- · · · · · · · ·		Gravelly SAND, fine grained sand with subrounded- coarse sand and gravel to 3/8-inch, predominantly
				feldspar and quartz in fine sand.
400	12:45			
480	12:45			
			495 – 505:	Brown Sandy CLAY, with est. 60% low plastic clay.
500	13:00			
			505 – 515:	Gray Silty SAND.
			515 - 565°	SAND, fine to coarse grained, moderately well
520			sorted, large	e fraction subrounded, w/est. 50% volcanic rock
			fragments (mostly basalt), 25% quartz, and 25% feldspar.
L	l	<u> </u>	l	

DRY VALLEY TEST WELL NO. 1 (DV-TW-1)

Logged by: D. Smith

Drilling Commenced: May 21, 2004

Driller: Humboldt Drilling

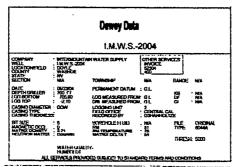
Drilling Method: Mud Rotary (6-inch diameter borehole)

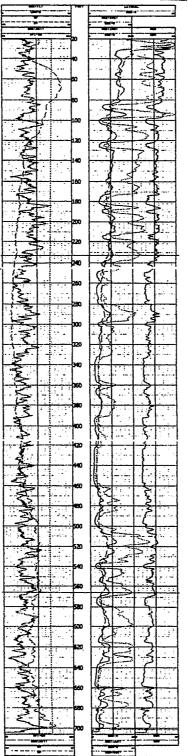
Page 3 of 3

540	13:45		540: Clay strata noted from E-log (est. less than 5-ft thick).
560			
			565 – 600: Gray Slightly Clayey Slightly Gravelly Silty SAND, subrounded to subangular, roughly even proportions of lithic
580	14:05		(volcanic – basalt), feldspar, and quartz. 575: Clay strata noted from E-log (est. less than 5-ft thick).
		• • • • • •	
600			600 – 610: Grayish Brn. Sandy CLAY.
			610 – 637: Grayish Brn. CLAYEY SAND w/est. 35% med.
620]	plastic clay.
640			637 – 658: Dark Brown Sandy CLAY, soft, low to med plastic, 70% fines.
040			70% liftes.
			658 – 685: Grayish Brn. Slightly Clayey Slightly Gravelly
660			SAND, predominantly subangular and coarse grained basalt particles.
680	16:00		
000	•		
			685 – 690: Gray Sandy CLAY w/est. 50% med. plastic clay.
700	16:20		690 – 702: Grayish Brn. Slightly Gravelly SAND, fine to coarse grained, mostly drk gray volcanic particles. 702 – 718: Sandy CLAY
720		-	
Neter			

Notes:

- 1. Total Depth Drilled = 718 ft.
- 2. Electric Logging by Dewey Data on 5-23-04, including natural gamma, SP, Point Resistance, Lateral Log, 16-inch Resistivity, and 64-inch Resistivity.
- 3. 6-inch diameter well completed to 700 ft in reamed borehole (12-inch diameter).
- 4. First water encountered at 5 ft below ground surface.
- 5. Static water level in completed well = 9.1 psi (22 ft above land surface).
- 6. Artesian flow of approx. 40 gpm (temperature = 85°F).





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DIVISION OF WATER RESOURCES

WELL DRILLER'S REPORT

Please complete this form in its entirety in accordance with NRS 534.170 and NAC 534.340

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1. OWNER In	termountal	Water Supply	<u>'</u>			ADDRESS AT	WELL LOCA	TION Dry Valley R	oad, Baso	of
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3.	WORK PE	RFORMED		4.		PROPOSED U	ISE	5.	WELL TYP	
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6.		LITHOLOGIC LO)G			8.	WE	LL CONSTRUCTION		
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Top Soil		1,L-2, 4) (p-1+ 4-4)	0	3	3			From	To	
Sand/grayel				12	9		13 Inches	0 Faot	100 Feet	
			12	20	8		9 7/8 Inches	100 Feet	718 Foot	
Sand/gravel			20	25	5			Feet	Feet	
Clay	Philippe seeded o 11 1 P F1 (4 to	., ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	25	26	1	,	CAS	SING SCHEDULE		
Sand/gravel			26	38	12	Size O.D.	Weight/Ft.	Well Thickness	i from	То
Clav			38	39	1_	(Inches)	(Pounds)	(Inches)	(Fool)	(Foot)
	nastnikinkalunu v tr			58	19	6 5/8		.188	+2	110
Clay		 	58	59		6 5/8 6 5/8		.188	250	510
Sand/some	gravel		59	80				.188	700	710
Cobbles			80	<u>85</u>		Perforations		i Mili Slot		
	ringers		85	96	11	Size per	foration .090			
Cobbies			96	101	5	From		10 feet to		50 feet
Gravelly clay Sand/gravel	 		101	104	3	rrom	<u>.ə</u>	10 feet to		UU feet
Clay			104	114	10	From		feet to		F 4
Gravel/cobb		· · · · · · · · · · · · · · · · · · ·	114	<u>11</u> 6	<u>2</u> 22	From		feet to		seet
Gravelly clay			138	176	38	Surface Seal:	X Yes	No	Seal Type:	
Clay			176	178		Depth of Seal	100		. Neet C	ement
Sandy clay			178	185	7	Placement Me	ethod: L&JPum □ Pou	iped	X Cemen	Grout
Cobbles				187	2	•			Concre	te Grout
Sandy clay			187	194	7		i: 🗓 Yes	L. No		
Gravelly san			194	218	24	110111350	:. <u></u>	feet to 718	***	1001
Clay			218	221	3	9.	W	ATER LEVEL		
Sand/gravel			221	226	5	Static water le	vel		feel below la	nd surface
Pink andesit	e		226	228	2	Water tempor	ature 83	G.P.M	И. З	P.S.I.
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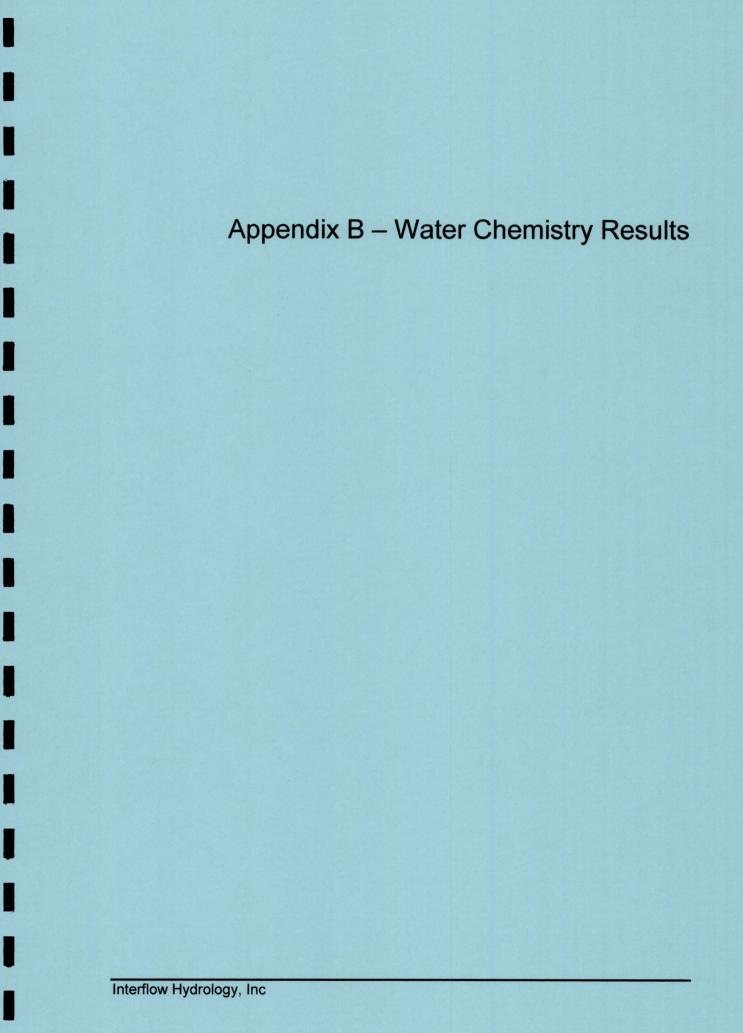
STATE OF NEVADA DIVISION OF WATER RESOURCES WELL DRILLER'S REPORT

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Page 2

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Sand/clay (gray)		254	257	3	11		Inches	From	To _	
Altered volcanics		257	261	4	1 -		hchas	Feet Fool	Feet	
Sandy clay		261	277	16	ll . <u> </u>		Inches	Feet	Feet	
Gravel	1	277	278	1	-				Feel	
Gravelly clay		278	285		31			ing schedule		
Cobbles		285	287	<u>7_</u>	Size O.D (Inches)		Weight/Fi. (Pounds)	(Inches)	From	To
Gravelty clay		287	292	<u>4</u> 5			((Fost)	(Foet)
Fractured basait		292	304	12	-	· -			 	
Clay		304	340	36	· · · · · · · · · · · · · · · · · · ·		 ·· -			
Sandy clay		340	357	90	Perforation				L	
Gravelly clay		357	397				ration			
Jan clay		397	406	40	Size	perfor	ation			
Graval		408		9	From			feet to		feet
Clay			419	13	From					feet
Gravel		500	500	81	From		* * * ********			
Sandy clay			503	3	From		• • • • • • • • • • • • • • • • • • • •			
Cand I		603	636	33	Surface Se		Yes [0-17	feet _
Coarse sand		536 551	551	15	Depth of 8	eai			Seal Type:	wheet
Clay (sticky)		637	837	<u>86</u>	Placement	Metho	d: 🔲 Pump	ed	Cement	Grout
Sandy clayleand		658	658	21_			Poure	d	Concret	e Grout
Sandy clay		702	702	44	Gravel Pac		☐ Yes	□ No		
		102	718	16.	From		·	feet to	-, ·	feet
					9.	_	W	ITER LEVEL		
					Static water		·		feet below lan	id surface
					Artesian fic Water tem			G.P.N	Λ	P.S.I.
								°F Quality		
					10.		DR	ILLER'S CERTIFIC	ATION	
ate completed 6/17/1904			 -	. 19	This well w	as drille knowled	ed under mu.	supervision and the n	eport is true to	the
MICH T				.10	-		•	Pump Co., Inc.		
	EST DATA			!/			V. Winnem	Contractor		
SPM Drs	ווי משוס TW Down	ump Te	ilA [□ nuoH) en	[]				Contractor	· ·	
(F481 B	elow Static)	- 11	(11001)				Nevada 89			•••
					INEUBO DY	Me SIS	s license nun te Contractor	's Board <u>56797</u>		
	T		·		Nevada drill Division of	er's lice Water	mse number Resources, i	issued by the he on-site driller	2235	····
	·	··			Signed					
					Dote	By drill	er performing	ectual drilling on-site of	confractor	





Laboratory **Analysis Report Report ID: 61646**

Interflow Hydrology, Inc.

Attn: Dwight Smith P.O. Box 1482

Truckee, CA 96160

Date:

7/9/2004

Client:

ITF-112

Taken by: PO #:

D. Smith

Sample ID:

Customer Sample ID

Date Sampled

Time Sampled

Date Received

•				- are sampred	a mile campion	Date Meeti, ca
S200406-2069	Dry Valley	Test Well #1		6/25/2004	12:15 PM	6/28/2004
			Units			Date
Parameter Parameter	Method	Result	Of Measure	MCL	Analyst	Analyzed
Alkalinity, Total	SM 2320 B	· 133	mg/L CaCO3		Kobza	7/4/2004
Alkalinity/Bicarbonate	SM 2320 B	122	mg/L CaCO3		Kobza	7/4/2004
Alkalinity/Carbonate	SM 2320 B	11	mg/L CaCO3		Kobza	7/4/2004
Alkalinity/Hydroxide	SM 2320 B	<2	mg/L CaCO3		Kobza	7/4/2004
Arsenic - ICP-MS	EPA 200.8	0.005	mg/L	0.01 mg/L	Li	7/7/2004
Barium - ICP-MS	EPA 200.8	0.003	mg/L	2.0 mg/L	Li	7/7/2004
Calcium - ICP-OES	EPA 200.7	3.3	mg/L	_	Layman	7/6/2004
Chloride - Ion Chromatography	EPA 300.0	8.8	mg/L	250 mg/L	Keller	7/1/2004
Color Apparent	EPA 110.2	<5	Color Units	15	Nava	6/30/2004
Copper - ICP-MS	EPA 200.8	< 0.001	mg/L	1.0 mg/L	Li	7/7/2004
Fluoride - Ion Chromatography	EPA 300.0	0.27	mg/L	2.0/4.0 mg/L	Keller	7/1/2004
Iron - ICP-OES	EPA 200.7	0.06	mg/L	0.3 mg/L	Layman	7/6/2004
Lead - ICP-MS	EPA 200.8	< 0.001	mg/L	0.015 mg/L	Li	7/7/2004
Magnesium - ICP-OES	EPA 200.7	<0.5	mg/L	125 mg/L	Layman	7/6/2004
Manganese - ICP-MS	EPA 200.8	0.011	mg/L	0.05 mg/L	Li	7/7/2004
MBAS Surfactants	SM 5540 C	< 0.05	mg/L	0.5 mg/L	Kobza	6/29/2004
Nitrate-N - Ion Chromatography	EPA 300.0	< 0.05	mg/L N	10 mg/L as N	Keller	7/1/2004
pН	SM 4500 H+B	8.54	pH Units	6.5 to 8.5	Kobza	7/4/2004
pH - Temperature	SM 4500 H+B	18.6	°C		Kobza	7/4/2004
Potassium - ICP-OES	EPA 200.7	0.6	mg/L		Layman	7/6/2004
Sodium - ICP-OES	EPA 200.7	67	mg/L		Layman	7/6/2004
Sulfate - Ion Chromatography	EPA 300.0	20	mg/L	500 mg/L	Keller	7/1/2004
Total Dissolved Solids	SM 2540 C	210	mg/L	500/1000 mg/L	Osterreicher	6/29/2004
Turbidity	SM 2130 B	0.5	NTU	_	Nava	6/30/2004
Zinc - ICP-MS	EPA 200.8	<0.01	mg/L	5 mg/L	Li	7/7/2004

SAMPLE WATER AS TESTED X DID ____ DID NOT MEET DRINKING WATER STANDARDS.

Page 1 of 2

1135 Financial Blvd. Reno, NV 89502-2348 Phone (775) 857-2400 FAX (775) 857-2404 sem@sem-analytical.com John C. Seher Special Consultant Quality Assurance Manager

John Kobza, Ph.D. Laboratory Director



Laboratory Analysis Report

Report ID: 61646

Interflow Hydrology, Inc.

Attn: Dwight Smith

P.O. Box 1482

Truckee, CA 96160

Date:

7/9/2004

Client:

ITF-112 D. Smith

Taken by:

PO #:

Approved By:

Sierra Environmental Monitoring, Inc

Date:

7/9/2004

This report is applicable only to the sample received by the laboratory. The liability of the laboratory is limited to the amount paid for this report. This report is for the exclusive use of the client to whom it is addressed and upon the condition that the client assumes all liability for the further distribution of the report or its contents.



Laboratory **Analysis Report Report ID: 61443**

Interflow Hydrology, Inc. Attn: Dwight Smith P.O. Box 1482 Truckee, CA 96160

Date:

6/28/2004

Client:

ITF-112

Taken by:

5 mg/L

D. Smith

PO#:

Sample ID:

Customer Sample ID

Date Sampled Time Sampled Date Received

				- and sumprou	- mile omilibree	Duce Trees, co
S200406-1482	Dry Valley	Test Well #1	•	6/17/2004	9:40 AM	6/17/2004
Parameter	Method	Result	Units Of Measure	MCL	Analyst	Date Analyzed
Alkalinity, Total	SM 2320 B	132	mg/L CaCO3		Kobza	6/24/2004
Alkalinity/Bicarbonate	SM 2320 B	124	mg/L CaCO3		Kobza	6/24/2004
Alkalinity/Carbonate	SM 2320 B	8	mg/L CaCO3		Kobza	6/24/2004
Alkalinity/Hydroxide	SM 2320 B	<2	mg/L.CaCO3		Kohza	6/24/2004

Kobza 0/24/2004 Arsenic - ICP-MS 0.005 **EPA 200.8** 0.01 mg/L mg/L Li 6/18/2004 Barium - ICP-MS **EPA 200.8** 0.004 mg/L 2.0 mg/L Li 6/18/2004 Calcium - ICP-OES **EPA 200.7** 3.4 mg/L Li 6/22/2004 Chloride - Ion Chromatography **EPA 300.0** 10 mg/L 250 mg/L Henderson 6/17/2004 Color Apparent **EPA 110.2** <5 **Color Units** 15 Kobza 6/19/2004 Copper - ICP-MS **EPA 200.8** 0.002 mg/L 1.0 mg/L Li 6/18/2004 Fluoride - Ion Chromatography **EPA 300.0** 0.21 Henderson mg/L 2.0/4.0 mg/L 6/17/2004 Iron - ICP-OES **EPA 200.7** 0.1 0.3 mg/L mg/L Li 6/22/2004 Lead - ICP-MS **EPA 200.8** < 0.001 0.015 mg/L mg/L Li 6/18/2004 Magnesium - ICP-OES **EPA 200.7** < 0.5 mg/L 125 mg/L Li 6/22/2004 Manganese - ICP-MS EPA 200.8 0.011 0.05 mg/L mg/L Li 6/18/2004 **MBAS Surfactants** SM 5540 C < 0.05 mg/L 0.5 mg/L Kobza 6/18/2004 Nitrate-N - Ion Chromatography EPA 300.0 0.14 mg/L N 10 mg/L as N Henderson 6/17/2004 SM 4500 H+B 8.43 pH Units 6.5 to 8.5 Kobza 6/24/2004 pH - Temperature SM 4500 H+B 20.8 °C Kobza 6/24/2004 Potassium - ICP-OES **EPA 200.7** 0.8 mg/L Li 6/22/2004 Sodium - ICP-OES **EPA 200.7** 67 Li ·mg/L 6/22/2004 Sulfate - Ion Chromatography **EPA 300.0** 20 500 mg/L mg/L Henderson 6/17/2004 **Total Dissolved Solids** SM 2540 C 240 500/1000 mg/L mg/L Osterreicher 6/21/2004 **Turbidity** SM 2130 B 1.1 NTU Kobza 6/19/2004

SAMPLE WATER AS TESTED _____ DID _ DID NOT MEET DRINKING WATER STANDARDS.

0.01

EPA 200.8

Page 1 of 2

1135 Financial Blvd. Reno, NV 89502-2348 Phone (775) 857-2400 FAX (775) 857-2404 sem@sem-analytical.com

mg/L

John C. Seher Special Consultant Quality Assurance Manager

6/18/2004

Li

John Kobza, Ph.D. Laboratory Director

Zinc - ICP-MS



Laboratory Analysis Report Report ID: 61443

Interflow Hydrology, Inc. Attn: Dwight Smith

P.O. Box 1482 Truckee, CA 96160 Date:

6/28/2004

Client:

ITF-112

Taken by:

D. Smith

PO #:

Approved By:

Sierra Environmental Monitoring, Inc

Date:

8/28/2004

This report is applicable only to the sample received by the laboratory. The liability of the laboratory is limited to the amount paid for this report. This report is for the exclusive use of the client to whom it is addressed and upon the condition that the client assumes all liability for the further distribution of the report or its contents.

Appendix C – Aquifer Test Data Interflow Hydrology, Inc

WELL ID: Dru Valley Test Well No. 1

INPUT Casing dia. (d_c) 8 Inch Annulus dia. (dw) 8 Inch Screen Length (L) 340 Feet water level (DTW) -21 Feet Top of Aquifer 0 Feet Base of Aquifer 700 Feet

Local ID: HML-Augmentation

Date: 6/24/2004

Time: 0:00

COMPUTED

Aquifer thickness =

700 Feet

34.49541 Feet/log10 Slope =

Input is consistent.

K = 0.16 Feet/Day T = 120 Feet²/Day

FLOW RATE

across screen - Open Hole

above screen - Cement

Aquifer Material - Fine Sand

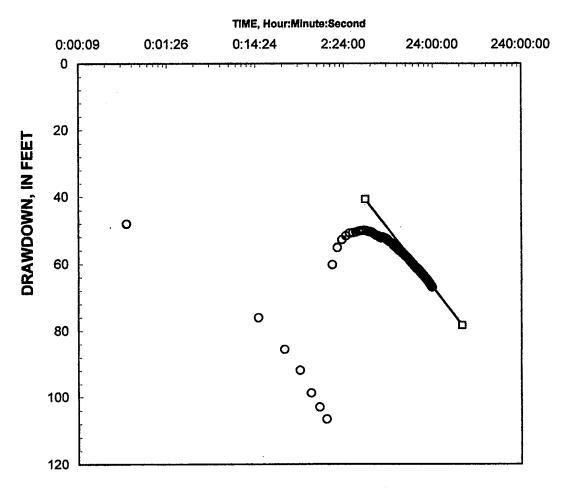
Construction:

Depths to:

Annular Fill:

113 GPM

K= 0.16 is less than likely minimum of 3 for Fine Sand



REMARKS:	Cooper-Jacob analysis of single-well aquifer tes
Analysis of 111 gpm data.	

	Reduced Data			. ар <u>э_</u> оооро	, cason cano.
	Time,	Water Level		Time,	Water Level
Coto (Date Hr:Min:Sec	Feet	Entry	Date Hr:Min:Sec	Feet
Entry 1	1/0/00 0:00:00	0.70	51	1/0/00 12:15:30	58.80
2	1/0/00 0:00:30	48.70	52	1/0/00 12:30:30	59.10
3	1/0/00 0:15:30	76.80	53	1/0/00 12:45:30	59.30
4	1/0/00 0:30:30	86.30	54	1/0/00 13:00:30	59.60
5	1/0/00 0:45:30	92.60	55	1/0/00 13:15:30	59.80
6	1/0/00 1:00:30	99.50	56	1/0/00 13:30:30	60.00
7	1/0/00 1:15:30	103.70	57	1/0/00 13:45:30	60.30
8	1/0/00 1:30:30	107.30	58	1/0/00 14:00:30	60.60
9	1/0/00 1:45:30	61.00	59	1/0/00 14:15:30	60.80
10	1/0/00 2:00:30	55.90	60	1/0/00 14:30:30	61.00
11	1/0/00 2:15:30	53.60	61	1/0/00 14:45:30	61.30
12	1/0/00 2:30:30	52.40	62	1/0/00 15:00:30	61.50
13	1/0/00 2:45:30	51.60	63	1/0/00 15:15:30	61.70
14	1/0/00 3:00:30	51.50	64	1/0/00 15:30:30	61.90
. 15	1/0/00 3:00:30	51.30	65	1/0/00 15:45:30	62.20
16	1/0/00 3:10:30	51.00	66	1/0/00 16:00:30	62.20
17	1/0/00 3:45:30	50.90	67	1/0/00 16:15:30	62.30
18	1/0/00 4:00:30	50.80	68	1/0/00 16:30:30	62.50
19	1/0/00 4:00:30	50.90	69	1/0/00 16:45:30	62.80
20	1/0/00 4:10:30	51.20	70	1/0/00 17:00:30	62.90
21	1/0/00 4:45:30	51.20	71	1/0/00 17:05:30	63.20
22	1/0/00 5:00:30	51.50	72	1/0/00 17:30:30	63.30
23	1/0/00 5:15:30	51.90	73	1/0/00 17:45:30	63.40
24	1/0/00 5:30:30	52.30	. 74	1/0/00 18:00:30	63.60
25	1/0/00 5:45:30	52.40	75	1/0/00 18:15:30	64.00
26	1/0/00 6:00:30	52.80	76	1/0/00 18:30:30	64.10
27	1/0/00 6:15:30	53.10	77	1/0/00 18:45:30	64.20
28	1/0/00 6:30:30	52.80	78	1/0/00 19:00:30	64.40
29	1/0/00 6:45:30	53.00	79	1/0/00 19:15:30	64.70
30	1/0/00 7:00:30	53.20	80	1/0/00 19:30:30	64.80
31	1/0/00 7:15:30	53.50	81	1/0/00 19:45:30	64.90
32	1/0/00 7:30:30	53.80	82	1/0/00 20:00:30	65.20
33	1/0/00 7:45:30	54.20	83	1/0/00 20:15:30	65.30
34	1/0/00 8:00:30	54.40	84	1/0/00 20:30:30	65.50
35	1/0/00 8:15:30	54.60	85	1/0/00 20:45:30	65.70
36	1/0/00 8:30:30	55.00	86	1/0/00 21:00:30	65.90
37	1/0/00 8:45:30	55.40	87	1/0/00 21:15:30	66.00
38	1/0/00 9:00:30	55.70	88	1/0/00 21:30:30	66.30
39	1/0/00 9:15:30	55.80	89	1/0/00 21:45:30	66.40
40	1/0/00 9:30:30	56.10	90	1/0/00 22:00:30	66.70
41	1/0/00 9:45:30	56.40	91	1/0/00 22:15:30	66.80
42	1/0/00 10:00:30	56.80	92	1/0/00 22:30:30	67.00
43	1/0/00 10:15:30	56.90	93	1/0/00 22:45:30	67.20
44	1/0/00 10:30:30	57.20	94	1/0/00 23:00:30	67.40
45	1/0/00 10:45:30	57.30	95	1/0/00 23:15:30	67.50
46	1/0/00 11:00:30	57.60			
47	1/0/00 11:15:30	57.90			
48	1/0/00 11:30:30	58.10			
49	1/0/00 11:45:30	58.40	,		
50	1/0/00 12:00:30	58.50			

WELL ID: Dry Valley Test Well No. 1 - Recovery Local ID: Intermountain TW-1

<u> </u>	NPUT			
Construction:				
Casing dia. (d _c)	6 Inch			
Annulus dia. (d _w)	12 Inch			
Screen Length (L) Depths to:	340 Feet			
water level (DTW)	-21 Feet			
Top of Aquifer	0 Feet			
Base of Aquifer	720 Feet			
Annular Fill:				
across screen – Open Hole				
above screen – Cement				
Aquifer Material F	ine Sand			

248 GPM

Date: 8/16/2004 Time: 15:40

COMPUTED

Aquifer thickness =

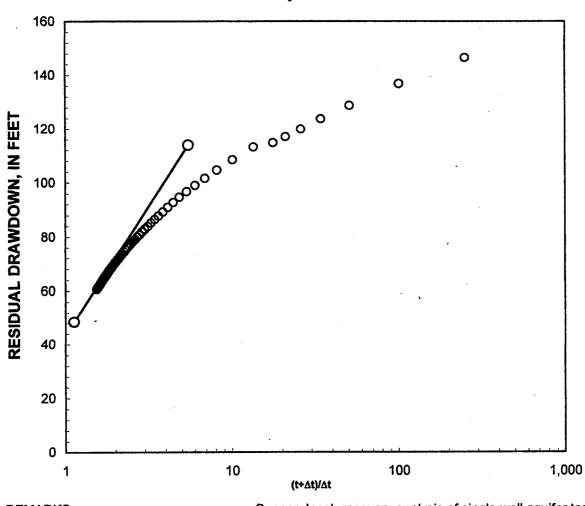
720 Feet

Slope = 95.05814 Feet/log10

Input is consistent.

K = 0.13 Feet/Day T = 92 Feet²/Day

K= 0.13 is less than likely minimum of 3 for Fine Sand



REMARKS:

FLOW RATE

Cooper-Jacob recovery analysis of single-well aquifer test

Recovery water level data for June test.

Water Level Feet 45.00 44.60 44.40 43.90 43.70 43.30 43.00 42.70 42.30 42.00 41.80 41.50 41.20 40.90

> 40.70 40.40 40.10 39.90 39.70

	Reduced Data			. == ,
	Time,	Water Level		Time,
Entry	Date Hr:Min:Sec	Feet	Entry	Date Hr.Min:Sec
1	1/0/00 15:40:00	-21.00	51	1/1/00 10:55:00
2	1/1/00 0:00:00	175.02	52	1/1/00 11:10:00
3	1/1/00 0:02:00	125.50	53	1/1/00 11:25:00
4	1/1/00 0:05:00	115.79	54	1/1/00 11:40:00
5	1/1/00 0:10:00	107.76	55	1/1/00 11:55:00
6	1/1/00 0:15:00	102.76	56	1/1/00 12:10:00
7	1/1/00 0:20:00	98.88	57	1/1/00 12:25:00
8	1/1/00 0:25:00	96.00	58	1/1/00 12:40:00
9	1/1/00 0:30:00	93.71	59	1/1/00 12:55:00
10	1/1/00 0:40:00	92.10	60	1/1/00 13:10:00
11	1/1/00 0:55:00	87.40	61	1/1/00 13:25:00
12	1/1/00 1:10:00	83.60	62	1/1/00 13:40:00
13	1/1/00 1:25:00	80.60	63	1/1/00 13:55:00
14	1/1/00 1:40:00	78.00	64	1/1/00 14:10:00
15	1/1/00 1:55:00	75.70	65	1/1/00 14:25:00
16	1/1/00 2:10:00	73.60	66 67	1/1/00 14:40:00
17 18	1/1/00 2:25:00 1/1/00 2:40:00	71.70 69.90	68	1/1/00 14:55:00 1/1/00 15:10:00
19	1/1/00 2:40:00	68.30	69	1/1/00 15:10:00
20	1/1/00 3:10:00	66.80	00	17 1700 10.29.00
21	1/1/00 3:25:00	65.50		
22	1/1/00 3:40:00	64.20		
23	1/1/00 3:55:00	63.00		•
24	1/1/00 4:10:00	62.00		
25	1/1/00 4:25:00	61.00		
26	1/1/00 4:40:00	59.90		
27	1/1/00 4:55:00	59.10		
28	1/1/00 5:10:00	58.10		
29	1/1/00 5:25:00	57.30		
30	1/1/00 5:40:00	56.50 55.70		
31	1/1/00 5:55:00	55.70 55.00		
32 33	1/1/00 6:10:00 1/1/00 6:25:00	54.20		
33 34	1/1/00 6:40:00	53.50		
35	1/1/00 6:55:00	52.90		
36	1/1/00 7:10:00	52.20		
37	1/1/00 7:25:00	51.70		
38	1/1/00 7:40:00	51.00		
39	1/1/00 7:55:00	50.50		
40	1/1/00 8:10:00	49.90		
41	1/1/00 8:25:00	49.50		
42	1/1/00 8:40:00	49.00		•
43 44	1/1/00 8:55:00 1/1/00 9:10:00	48.40 48.00		
44 45	1/1/00 9:10:00	47.50		
46	1/1/00 9:40:00	47.10		
47	1/1/00 9:55:00	46.70		
48	1/1/00 10:10:00	46.30		
49	1/1/00 10:25:00	45.80		
50	1/1/00 10:40:00	45.40		

WELL ID: Dry Valley Test Well No. 1

INPUT	_
1141 01	

0.001 d'less

Construction:					
Casing dia. (d _c)	6	Inch			
Annulus dia. (d _w)	12	Inch .			
Screen Length (L)	340	Feet			
Depths to:					
water level (DTW)	-21	Feet			
Top of Aquifer	0	Feet			
Base of Aquifer	720	Feet			
Annular Fill:					
across screen Open Hole					
above screen – Cement					
Aquifer Material Fine Sand					
FLOW RATE	304	GPM			

Assumed Storage =

Local ID: Intermountain TW-1

Date: 8/16/2004 Time: 13:00

COMPUTED

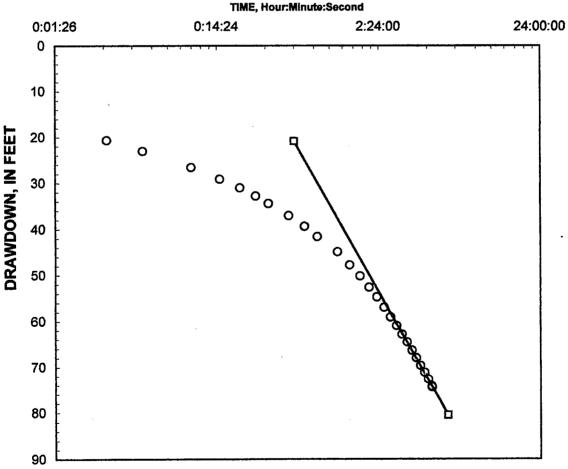
Aquifer thickness =

720 Feet

Slope = 62.90084 Feet/log10

Input is consistent.

K =	0.24 Feet/Day
T =	170 Feet²/Day



REMARKS:

Cooper-Jacob analysis of single-well aquifer test

Third step of second aquifer test. Depths to ground water reported below starting artesian head of 22 feet above land surface (9.1 psi).

Reduced Data					
	Time,	Water Level			
Entry	Date Hr:Min:Sec	Feet			
1	1/0/00 0:00:00	100.60			
2	1/0/00 0:03:00	121.20			
3	1/0/00 0:05:00	123.62			
4	1/0/00 0:10:00	127.18			
5	1/0/00 0:15:00	129.70			
6	1/0/00 0:20:00	131.60			
7	1/0/00 0:25:00	133.41			
· 8	1/0/00 0:30:00	135.04			
9	1/0/00 0:40:00	137.65			
10	1/0/00 0:50:00	139.98			
11	1/0/00 1:00:00	142.22			
12	1/0/00 1:20:00	145.50			
13	1/0/00 1:35:00	148.40			
14	1/0/00 1:50:00	150.80			
15	1/0/00 2:05:00	153.30			
16	1/0/00 2:20:00	155.40			
17	1/0/00 2:35:00	157.60			
18	1/0/00 2:50:00	159.70			
19	1/0/00 3:05:00	161.60			
20	1/0/00 3:20:00	163.50			
21	1/0/00 3:35:00	165.20			
22	1/0/00 3:50:00	167.00			
23	1/0/00 4:05:00	168.60			
24	1/0/00 4:20:00	170.30			
25	1/0/00 4:35:00	171.80			
26	1/0/00 4:50:00	173.30			
27	1/0/00 5:05:00	174.80			

WELL ID: Dry Valley Test Well No. 1 - Recovery Local ID: Intermountain TW-1

<u>IN</u>	IPU I				
Construction:					
Casing dia. (d _c)	6 Inch				
Annulus dia. (d _w)	12 Inch				
Screen Length (L)	340 Feet				
Depths to:					
water level (DTW)	-21 Feet				
Top of Aquifer	0 Feet				
Base of Aquifer	700 Feet				
Annular Fill:					
across screen - O	oen Hole				
above screen Cement					
Aquifer Material Fine Sand					
FLOW RATE	248 GPM				

BIDLIT

Date: 8/16/2004 Time: 15:40

COMPUTED

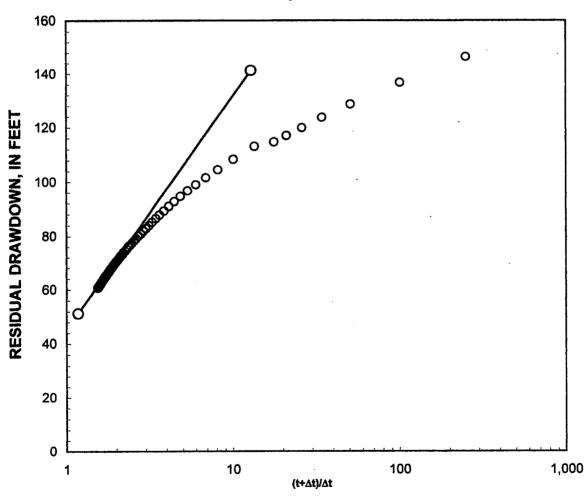
Aquifer thickness = 700 Feet

Slope = 86.37236 Feet/log10

Input is consistent.

0.14 Feet/Day K = T = 100 Feet2/Day

K= 0.14 is less than likely minimum of 3 for Fine Sand



REMARKS:

Cooper-Jacob recovery analysis of single-well aquifer test

Recovery water level data from August test.

	Reduced Data				
	Time,	Water Level		Time,	Water Level
Entry	Date Hr:Min:Sec	Feet	Entry	Date Hr:Min:Sec	Feet
1	1/0/00 15:40:00	-21.00	51	1/1/00 10:55:00	45.00
2	1/1/00 0:00:00	175.02	52	1/1/00 11:10:00	44.60
3	1/1/00 0:02:00	125.50	53	1/1/00 11:25:00	44.40
. 4	1/1/00 0:05:00	115.79	54	1/1/00 11:40:00	43.90
5	1/1/00 0:00:00	107.76	55	1/1/00 11:55:00	43.70
6	1/1/00 0:15:00	102.76	56	1/1/00 12:10:00	43.30
7	1/1/00 0:20:00	98.88	57	1/1/00 12:25:00	43.00
8	1/1/00 0:25:00	96.00	58	1/1/00 12:40:00	42.70
9	1/1/00 0:30:00	93.71	59	1/1/00 12:55:00	42.30
10	1/1/00 0:30:00	92.10	60	1/1/00 13:10:00	42.00
11	1/1/00 0:45:00	87.40	61	1/1/00 13:25:00	41.80
12	1/1/00 0:33:00	83.60	62	1/1/00 13:40:00	41.50
13	1/1/00 1:25:00	80.60	63	1/1/00 13:55:00	41.20
		78.00	64	1/1/00 14:10:00	40.90
14	1/1/00 1:40:00		65	1/1/00 14:10:00	40.90
15	1/1/00 1:55:00	75.70		1/1/00 14:25:00	
16	1/1/00 2:10:00	73.60 71.70	66 67	1/1/00 14:40:00	40.40 40.10
17 18	1/1/00 2:25:00 1/1/00 2:40:00	71.70 69.90	68	1/1/00 14:55:00	39.90
19	1/1/00 2:40:00	68.30	69	1/1/00 15:10:00	39.70
20	1/1/00 3:10:00	66.80	09	17 1700 15.25.00	39.70
21	1/1/00 3:10:00	65.50			
22	1/1/00 3:25:00	64.20			
23	1/1/00 3:40:00	63.00			
24	1/1/00 4:10:00	62.00			
25	1/1/00 4:25:00	61.00			
26	1/1/00 4:40:00	59.90		• ,	
27	1/1/00 4:55:00	59.10			
28	1/1/00 5:10:00	58.10			
29	1/1/00 5:16:00	57.30			
30	1/1/00 5:40:00	56.50			
31	1/1/00 5:55:00	55.70			
32	1/1/00 6:10:00	55.00			
33	1/1/00 6:25:00	54.20			
34	1/1/00 6:40:00	53.50			
35	1/1/00 6:55:00	52.90			
36	1/1/00 7:10:00	52.20		4	
37	1/1/00 7:25:00	51.70			
38	1/1/00 7:40:00	51.00			•
39	1/1/00 7:55:00	50.50			
40	1/1/00 8:10:00	49.90			
41	1/1/00 8:25:00	49.50			
42	1/1/00 8:40:00	49.00			
43	1/1/00 8:55:00	48.40			
44	1/1/00 9:10:00	48.00	•		
45	1/1/00 9:25:00	47.50			
46	1/1/00 9:40:00	47.10			
47	1/1/00 9:55:00	46.70			
48	1/1/00 10:10:00	46.30		, *	
49 50	1/1/00 10:25:00 1/1/00 10:40:00	45.80 45.40			
อบ .	1/1/00 10:40:00	40.40			

WELL ID: Dry Valley Test Well No. 1 - Step Drawdow

	INPUT
Construction:	
Casing dia. (d _c)	6 Inch
Annulus dia. (d _w)	12 Inch
Screen Length (L)	340 Feet
Depths to:	
water level (DTW)	-21 Feet
Top of Aquifer	0 Feet
Base of Aquifer	720 Feet
Annular Fill:	
across screen -	Gravel
above screen	Cement
Aquifer Material	Fine Sand
ASSUMED S =	0.0004 d'less

Local ID: Dry Valley Test Well No. 1 Date: 8/16/2004

Time: 1:00

COMPUTED

Aquifer thickness = 700 Feet

Input is consistent.

 K =
 0.2 Feet/Day

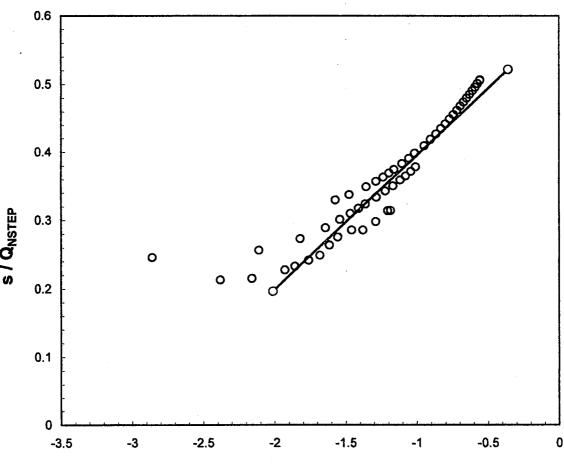
 T =
 200 Feet2/Day

 S =
 0.0004 d'less

 K_{annular} =
 3 Feet/Day

 Skin =
 -0.6 d'less

K= 0.2 is less than likely minimum of 3 for Fine Sand

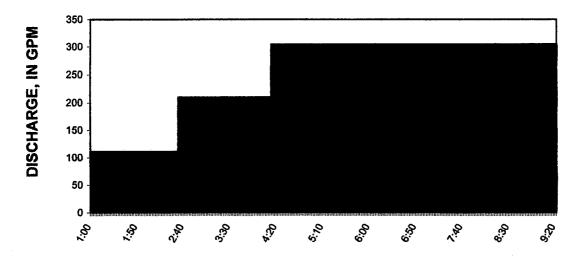


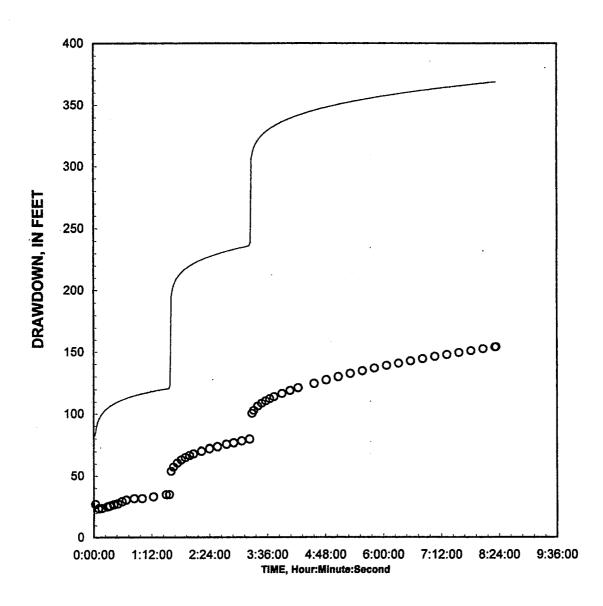
 $\sum_{i=1}^{NSTEP} \frac{Log(\Delta t_i) \Delta Q_i}{Q_{NSTEP}}$

REMARKS:

Step-drawdown analysis of single-well aguifer test

KANNULAR is estimated by fitting simulated drawdowns to measured drawdowns in a secondary plot. A reasonable storage value must be assigned by the user because storage and KANNULAR cannot be estimated independently. The estimate of T is not affected by changes in estimates of storage and KANNULAR.





Test	Reduced Data			,	,
	Time,	Water Level		Time,	Water Level
Entry	Hr:Min:Sec	Feet	Entry	Hr:Min:Sec	Feet
1	1:00:00	21.00	51	8:19:00	168.60
2	1:02:00	48.30	52	8:34:00	170.30
3	1:06:00	44.65	53	8:49:00	171.80
. 4	1:10:00	44.88	54	9:04:00	173.30
5	1:17:00	46.26	55	9:19:00	174.80
. 6	1:20:00	46.85	56	9:20:00	175.02
7	1:25:00	47.82			
8	1:30:00	48.64			
9	1:35:00	50.28			
10	1:40:00	51.60			
11	1:50:00	52.74			
12	2:00:00	52.74			
13	2:14:00	54.09			
14	2:30:00	55.86			
15	2:34:00	55.90			
16	2:36:00	74.83			
17	2:39:00	78.35		•	
18	2:44:00	81.69			
19	2:49:00	84.25			
20	2:54:00	86.10			
21	2:59:00	87.67			
22	3:04:00	88.95			
23	3:14:00	91.07			
24	3:24:00	93.03			
25	3:34:00	94.65		•	
26	3:45:00	96.48			
27	3:54:00	97.73			
28	4:04:00	99.18			
29	4:14:00	100.60			
30	4:17:00	121.20	•		
31	4:19:00	123.62			
32	4:24:00	127.18			
33	4:29:00	129.70			
34 35	4:34:00	131.60			
36	4:39:00 4:44:00	133.41 135.04			
37	4:54:00	137.65			
38	5:04:00	139.98			
39	5:14:00	142.22			
40	5:34:00	145.50			
41	5:49:00	148.40			
42	6:04:00	150.80			
43	6:19:00	153.30			
44	6:34:00	155.40			
45	6:49:00	157.60			
46	7:04:00	159.70			
47	7:19:00	161.60		,	
48	7:34:00	163.50			
49	7:49:00	165.20			
50					
50	8:04:00	167.00			. •