

**JULY 1997** 



## **WASHOE COUNTY**

DEPARTMENT OF WATER RESOURCES

UTILITY SERVICES DIVISION

4930 ENERGY WAY RENO, NEVADA 89502



### DESERT SPRINGS WATER SYSTEM MONITORING WELLS 5 AND 6 CONSTRUCTION

**JULY 1997** 

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### TABLE OF CONTENTS

Summary	••••••••		*************	•••••	••••	• • • • • • • • • • • • • • • • • • • •	1
Drilling Operations							
Well Construction							
DSMW5	•••••	•••••••	•••••	•••••		#C	4
DSMW6	•••••	•••••	•••••	····	••••••	•••••	6
Borehole Samples							
Water Quality							
Conclusions	•	•••••	***************************************		•••••		-12
References		••••••••			•••••	••••••	13
Appendix	••••••	•••••	•••••	••••		•••••	· 14

Project Cost Summary
Well Driller's Reports
Water Quality Analyses
Borehole Sample Sieve Analyses

## TABLES AND FIGURES

TAB	LES	Page
1	Well Construction Summary	. 4
2	Formation Water Samples	8
. 3	Water Quality Summary	9
4	Production Well Recommendations	11
FIGU	J <b>ŖES</b>	
. 1	Monitoring Well Location Map	. 2
2	DSMW5 Log & Construction	. 5
3 ·	DSMW6 Log & Construction	7
4	Piper Diagram	. 10
5	Potentiometric Surface Man	. 11

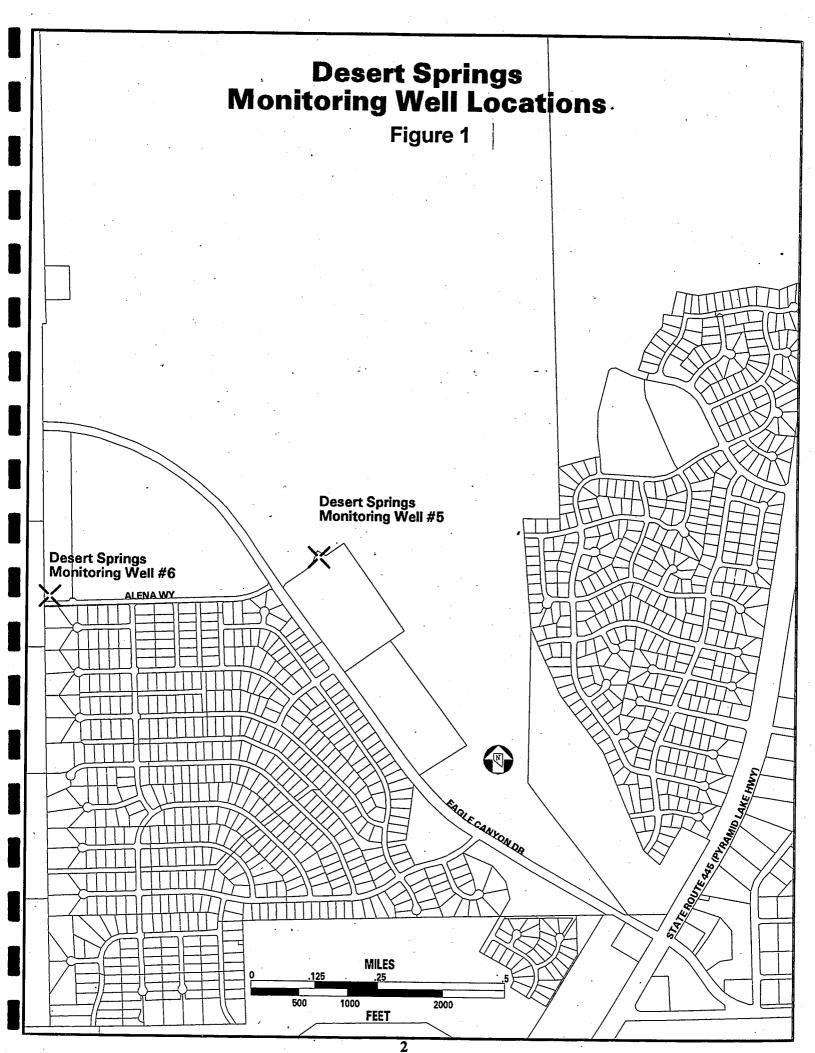
### **Summary**

The Spanish Springs Village subdivision service area has increased beyond the current peak day production well capacity of the Desert Springs Water system. The water system is operated by the Washoe County Department of Water Resources, Utility Services Division. At least one 500+ gallon per minute(gpm) production well is needed to increase system supply. The targeted well capacity is obtainable, however water quality problems in the west valley area limit suitable production well sites. Water quality problems in the alluvial aquifer were identified as a result of the construction and testing of monitoring wells in 1993 for the water resource study "Hydrogeology and Simulated Effects of Urban Development on Water Resources of Spanish Springs Valley" prepared by the United States Geological Survey (USGS). Initial sampling showed ground water in several west side monitoring wells exceeded the State of Nevada primary and secondary drinking water maximum contaminant levels(mcl) for arsenic(As) and nitrate(NO³-N). Two monitoring wells were constructed to find a production well site which met the following requirements; sufficient well yield with As, NO³ levels and total water quality that met drinking water standards. Figure 1 is a map showing DSMW5, DSMW6 and nearby County monitoring and production wells.

Lang Exploratory Drilling of Elko, NV started the drilling project on January 9, 1997 and completed well construction on January, 21 1997. The wells were drilled by the dual tube, reverse air method. Monitoring well DSMW5 was drilled east of Alena Way on Washoe County School District property and DSMW6 was drilled northwest of Spanish Springs Village, Unit 7 on HAWCO property. DSMW5 was drilled to a depth of 680 feet and constructed to a total depth of 670 feet. DSMW6 was drilled to a depth of 610 feet and constructed to a total depth of 525 feet. Water quality samples for As and NO<sup>3</sup>-N were collected from DSMW5 at borehole depths of 180, 410, 580 and 680 feet. NO<sup>3</sup>-N concentrations ranged from 1-4 parts per million(ppm) and arsenic concentrations ranged between 0.08-0.18 ppm. Water quality samples for As and NO<sup>3</sup>-N were collected from DSMW6 at borehole depths of 200, 260, 340, 400, 460 560 and 610 feet. NO<sup>3</sup>-N concentrations ranged from 0-0.3 parts per million(ppm) and As concentrations ranged from 0.60-0.12 ppm. Formation water temperature ranged between 60-100 degrees Fahrenheit (°F) in both wells. Well yield for each well ranged from 50-200 gpm per sample.

The drilling project identified two sites that meet two of the three criteria necessary for production well construction; satisfactory well yield and nitrate levels that meet State of Nevada drinking water standards. Arsenic levels in both wells exceeded maximum contaminant levels throughout the borehole. The potential yield of the wells and the urgency for increased well capacity in the Desert Springs Water System prompted investigation of alternatives for water quality enhancement and arsenic removal at each site. PROSYS Corporation was contacted about arsenic removal since they are experienced in designing arsenic removal systems for high volume well systems. PROSYS suggested implementing a pilot testing program for arsenic removal at one of the monitoring wells. The pilot testing program was not pursued due to the program cost of approximately \$22,000.00.

Monitoring well DSMW5 has the potential for a shallow production well from 0-230 feet and a deep production well from 0-660 feet. Estimated well yield for the shallow well is 200-300 gpm and 500+ gpm for the deep well. An advantage of a shallow production well is the temperature of



well discharge will be kept below 70 degrees °F, which allows better mixing with lower temperature water in the existing Desert Springs system. DSMW6 could be completed as a 600 foot production well with an estimated well yield of 500+ gpm.

At the time of monitoring well completion, the potential for a long term water exchange agreement between Westpac Utilities and the County for wholesale water purchase and delivery to Spanish Springs Valley is being pursued by both entities. Construction of new production wells, especially in areas where water quality is a concern, is not a option that is currently proposed by staff. Production well construction can always be considered in the future when or if a wholesale agreement reaches completion.

#### **Drilling Operations**

Monitoring well construction was done by Lang Exploratory Drilling of Elko, NV. A Lang modified, top head drive, air rotary drilling rig was used for borehole drilling. 6 1/4 inch boreholes were drilled at each well using the dual tube, reverse air rotary method. The boreholes were drilled with tri-cone chisel or button bits. The dual tube drilling method was selected since it allows at point collection of formation samples with minimal circulation of borehole cuttings. The method also allowed instantaneous well yield approximation of a selected zone of the borehole and discrete formation water sampling with minimal mixing or circulation from previously drilled zones. Rapid drilling rates can be achieved with this method with the slowest day of drilling producing 300 feet of borehole.

The drilling fluid consisted of potable water from the Desert Springs Water System and Baroid Quik-Foam foaming agents. When it became necessary to clean the borehole of accumulated cuttings, the density of the drilling fluid was increased using E-Z Mud synthetic organic polymer. Twice during drilling of DSMW5 Baroid Qik-Gel high yield, bentonite clay was mixed with clean water in a portable mud pit in order to drill through saturated, fine sand layers. A cyclone splitter was used to discharge drilling fluid, formation water and remove borehole cuttings. All borehole samples were collected at the discharge end of the cyclone splitter.

Formation samples were collected during borehole drilling at five foot intervals with samples bagged and labeled a minimum of every ten feet or at a major formation change. Borehole geophysics logging of both wells was done by Welenco, Bakersfield, CA. A guarded resistivity, long and short normal electric log, spontaneous potential and caliper log were originally specified for each well. Long and short normal electric were the only logs done at DSMW6 because of Welenco equipment failure. A natural gamma log was added to the contracted work by Welenco at DSMW5 as an exchange for the equipment failure at DSMW6. Water quality and formation sampling, well design and construction supervision were done by Washoe County Utility Services Division (WCUSD) personnel.

#### Well Construction

The monitoring wells were constructed using 2-1/2 inch black steel pipe with steel caps threaded on the bottom. Perforated pipe with three 3/32" X 3" inch double mill slots per foot was used in each

well. All pipe joints were connected using threaded couplings. All wells were installed with a gravel envelope consisting of well rounded, siliceous 1/4" X 1/8" gravel supplied by Silica Resources Inc., Auburn, California. Neat cement sanitary seals were installed with a grout pump and tremmie pipe. A six inch diameter protective casing and locking cap were cemented in place at each well head.

All monitoring wells were developed by air after the sanitary seals had hardened for a minimum of 12 hours. Well development was accomplished using the drilling rig air compressor to blow high velocity air through a one inch steel development line with a five foot perforated development tool attached to the bottom. The slotted interval of each well was developed by surging in 10-20 foot sections until clear discharge was produced. A well construction summary is found in Table 1.

Well	Total Depth Feet	Cased Depth Feet	Blank Interval Feet	Slotted Interval Feet	Static W. L. Feet below - m.p.	Seal Depth Feet
DSMW5	680	672	462	210	34.46	130
DSMW6	620	525	273	252	77.20	100

Table 1
Well Construction Summary

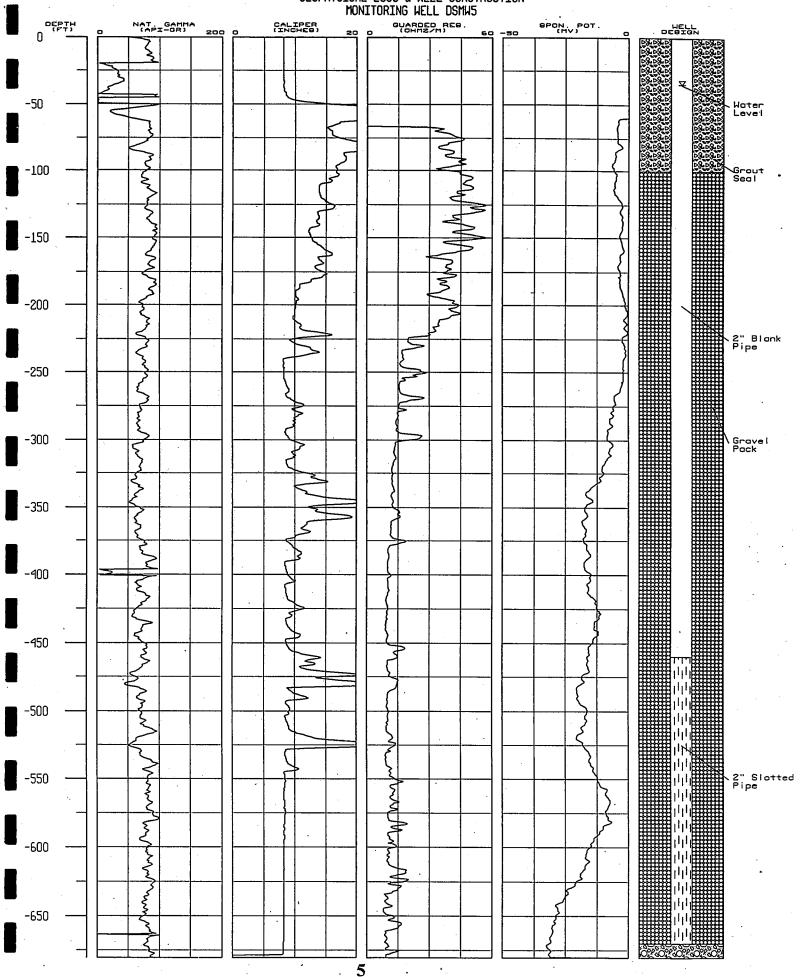
The monitoring wells were drilled in valley basin fill comprised of alluvium and lacustrine sediments. Bedrock was not encountered in either well. The boreholes were continuously sampled and logged by WCUSD personnel. Well driller's reports for each well are in the appendix.

#### DSMW5

Alluvium containing sub-rounded, moderate to well sorted granitic sand with intermittent small, sub-angular to sub-rounded mafic, volcanic gravel stringers was drilled from 0 to 224 feet. Sample volume of gravel where encountered was 10-30%. Pliable, sticky blue and gray lacustrine clay was drilled from 225 to 450 feet. Fine to medium grained, moderately sorted and rounded andesite sand with intermittent silty clay and volcanic gravel lenses was drilled from 450 to 680 feet. Sample volume of gravel was 5-15%. The andesite sand drilled from 630-680 feet became finer as drilling progressed to borehole bottom.

Short and long normal electric, guarded resistivity, spontaneous potential, six foot lateral and natural gamma logs were done at DSMW5. Figure 2 is a borehole log and well construction diagram for DSMW5. A shallow, uniform sand aquifer was drilled from 0 to 224 feet that has a resistivity ranging from 30-60 ohmeters<sup>2</sup>/meter. Logging shows the large clay zone from 225 to 450 feet has a consistent 10-15 ohmeters<sup>2</sup>/meter resistivity that separates a shallow and deep aquifer. The deep aquifer from 450 to 680 feet is primarily composed of fine, mafic sand with a 10-20 ohmeters<sup>2</sup>/meter resistivity. The deep aquifer formation had higher water production during drilling than the higher resistivity, shallow aquifer formation found above 230 feet(see Borehole Samples, Table 2). Overall, aquifer formations in DSMW5 have a slightly higher resistivity and higher at point formation discharge than the formations drilled at DSMW6.

FIGURE 2
GEOPHYSICAL LOGS & WELL CONSTRUCTION
MONITORING WELL DSMW5



#### DSMW6

Alluvium containing coarse granitic and felsic volcanic sand with intermittent clay layers from 5 to 20 feet thick, was drilled from 0 to 150 feet. Pliable, sticky to hard, brown and blue /gray clay was drilled from 150 to 250 feet. Medium to coarse grained sub-round volcanic and granitic sand, with intermittent clay zones was drilled from 250 to 480 feet. Small to coarse gravel with a sample volume between 10-30% was drilled in this section between 250 and 300 feet. Moderately sorted, mafic volcanic sand with stringers of sandy clay and small gravel was drilled from 480 to 620 feet. Sample volume of gravel ranged between 10-25%.

Short and long normal electric, single point and spontaneous potential logs were done at DSMW6. A guarded resistivity log was not conducted at this site due to logging equipment failure. Figure 3 is a borehole log and well construction diagram for DSMW6. The resistivity logs showed large clay zones with 5-10 ohmeters²/meter resistivity from 150 to 230 feet and 300 to 332 feet. Thinner, intermittent clay beds with a similar low resistivity were found throughout the borehole. The primary water bearing formations from 330 to 520 feet have a resistivity of 10-15 ohmeters²/meter. The finer volcanic sand and sandy clay formation from 520 to 620 feet have a resistivity of 5-10 ohmeters²/meter. The water bearing formations identified in DSMW6 by the borehole geophysics, have an overall low formation resistivity however the high discharge samples collected during drilling suggest a reasonably high formation permeability(Borehole Samples, Table 2).

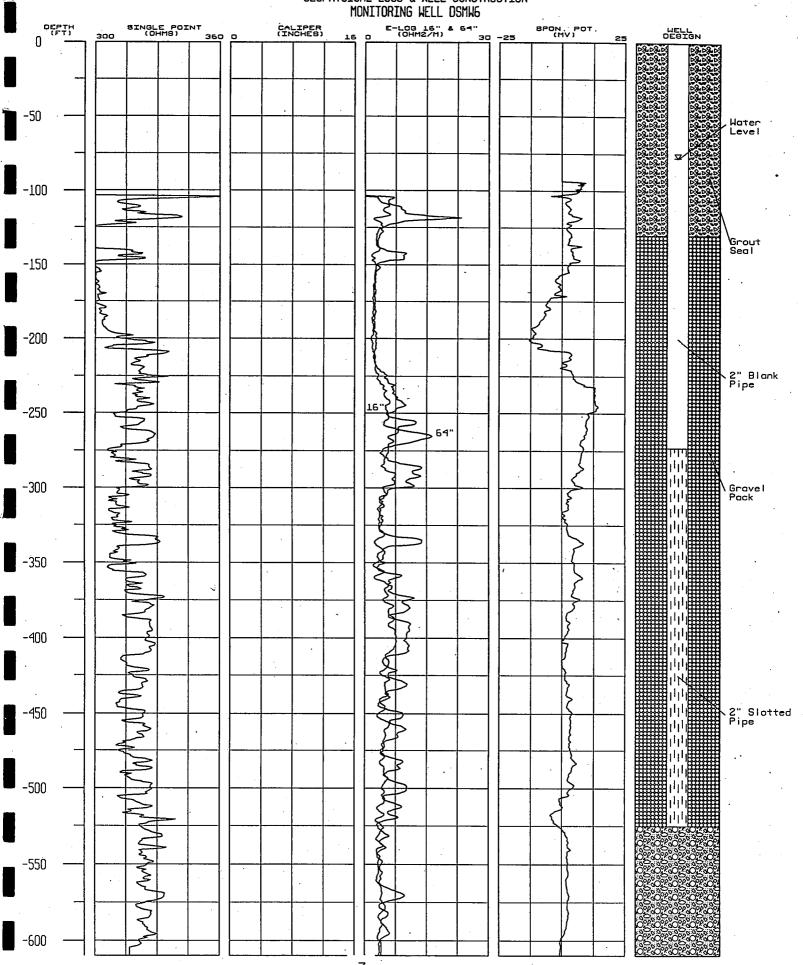
Five borehole samples were collected from each well for sieve analysis so a screen slot size and appropriate gravel filter pack could be selected for production well construction. Sieve analysis were performed by Roscoe Moss Company, Sacramento, CA. A screen size of 50 slot (0.05") was recommended for DSMW5 with a gravel filter pack of #6 x #8 and a screen size of 80 slot (0.08") was recommended for DSMW6 with a 1/8" x 1/4" gravel filter pack. Screen size was selected to allow 90% filter pack retention. Complete sieve analyses are found in the appendix.

#### **Borehole Samples**

The primary goal of drilling the monitoring wells by the dual tube reverse method was the ability to collect a water sample from a discrete portion of the aquifer with minimal delays in operation and few equipment changes. Water samples were collected from various borehole depths in order to verify if arsenic or Nitrate-N concentrations were located in isolated formations or continuous throughout the borehole. Water quality samples were collected at points specified by the supervising geologist with selection criteria for sampling based on adequate formation discharge, discharge clarity and lithology. At point formation discharge rate, formation water temperature and a field measurement for NO<sup>3</sup>-N were also collected at each sampling.

Nitrate and arsenic samples were analyzed by Sierra Environmental Monitoring (SEM) of Reno, Nevada. Field measurements for nitrate were made using a LaMotte Field Testing Kit for NO<sup>3</sup>-N with a range of 0-18 ppm. Discharge measurements were estimated by bucket test at the discharge end of the cyclone splitter. Temperature was measured using a standard glass thermometer. Table 2 shows a summary of field parameters measured and SEM laboratory results for the borehole water samples collected from each site.

FIGURE 3
GEOPHYSICAL LOGS & WELL CONSTRUCTION
MONITORING WELL DSMW6



	Sample Depth	NO <sup>3</sup> -N Field	NO <sup>3</sup> -N(SEM)	Arsenic	Temperature	At Point Discharge
Well	Feet	ppm	mg/L	mg/L	°F	gpm
DSMW5	180	2-3	2.1	0.085	65	60
	410	6-7	4.2	0.098	60	100
	580	2-4	2.4	0.11	75	200
·	680	1-2	<1	0.18	92	180-200
DSMW6	200	0-1	0.3	0.088	n/a	25-30
	260	0-1	<0.1	0.12	80	50-60
•	340	0-1	<0.1	0.068	90	85
	400	0-1	<0.1	0.061	90	100
	460	0-1	<0.1	0.065	93	150
	560	0-1	<0.1	0.076	95	150
. <u></u>	610	0-1	<0.1	0.078	n/a	150+

Table 2
Formation Water Samples

Borehole sampling, at DSMW5 and DSMW6 did not identify a specific formation or borehole section that is the primary source for nitrate and arsenic. Arsenic concentrations in DSMW6 remained relatively consistent and appear to be associated with the elevated thermal water gradient throughout the borehole. This suggests that the well is located near a lineament that conveys hydrothermal formation water along a structure that could range from an isolated basin feature to inter-basin in size. A convenient structure for water movement is the regional Warms Springs fault zone that trends north along Hungry Ridge at the western edge of Spanish Springs Valley (Bell, 1969), approximately 1/2-1 mile away from DSMW6. Nitrate concentration did not exceed 0.3 mg/L throughout the borehole, indicating the well penetrates an aquifer which is not in contact with nitrate bearing lacustrine sediments seen in existing monitoring wells to the north. Nitrate contamination in DSMW6 from domestic septic systems in the HAWCO and Sky Ranch subdivisions should be minimized by the well's upgradient location.

DSMW5 had nitrate levels that did not exceed drinking water maximum contaminant levels and decreased with drilling depth. The clay unit provides a natural vertical barrier that restricts downward migration of nitrate between the shallow and deep aquifer. Nitrate levels in the clay aquitard penetrated by DSMW5 were measured at 4 mg/L(Table 2, sample DSMW5-410). The nitrate value measured in the clay unit can be considered a baseline or natural value so a nitrate increase above this level in the shallow aquifer could be attributed to man made sources such as septic tank and leach field discharge. The final sample taken at DSMW5 (680 feet) showed the nitrate level had dropped to a similar concentration level measured in DSMW6, indicating that a common formation between the two wells exists. Arsenic levels increased as borehole depth increased, but stayed within a range of 0.10 mg/L. The uniformity of the arsenic concentration and sample water temperature throughout the borehole show DSMW5 is affected by the same geologic structure and thermal setting responsible for high arsenic levels in DSMW6.

#### Water Quality

Water quality samples for inorganic compounds, which included testing for trace metals and routine mineral analysis, were collected at both monitoring wells. Samples were collected from both wells

upon completion of air development. Water samples for inorganic compounds were collected in one gallon plastic milk bottles and 60 milliliter(ml) plastic bottles preserved with nitric and sulfuric acid. Water samples were analyzed by the Nevada State Health Lab in Reno, Nevada.

DSMW5 and DSMW6 meet State of Nevada primary and secondary drinking water standards for all parameters tested except arsenic and nitrate-N. The current(5/97) State of Nevada maximum contaminant level for arsenic is 0.05 mg/L and 10 mg/L for nitrate-N. Complete water quality analyses for each well are found in the appendix. A general water quality summary for each well is found in Table 2. Constituents that do not meet primary drinking water standards are shaded. Overall water quality is better at DSMW6 than DSMW5 which is presumably caused by the partial penetration of lacustrine sediments by DSMW5.

Well	TDS	NitN	SO <sup>4</sup>	Cl	HCO <sup>3</sup>	Fe	Na	K	Ca	Fl	As
DSMW5	337	0.1	69	14	144	17	108	1	4	2.12	0.117.
DSMW6	199	0.0	18	7	95	0.13	72	0	1	0.93	0.06

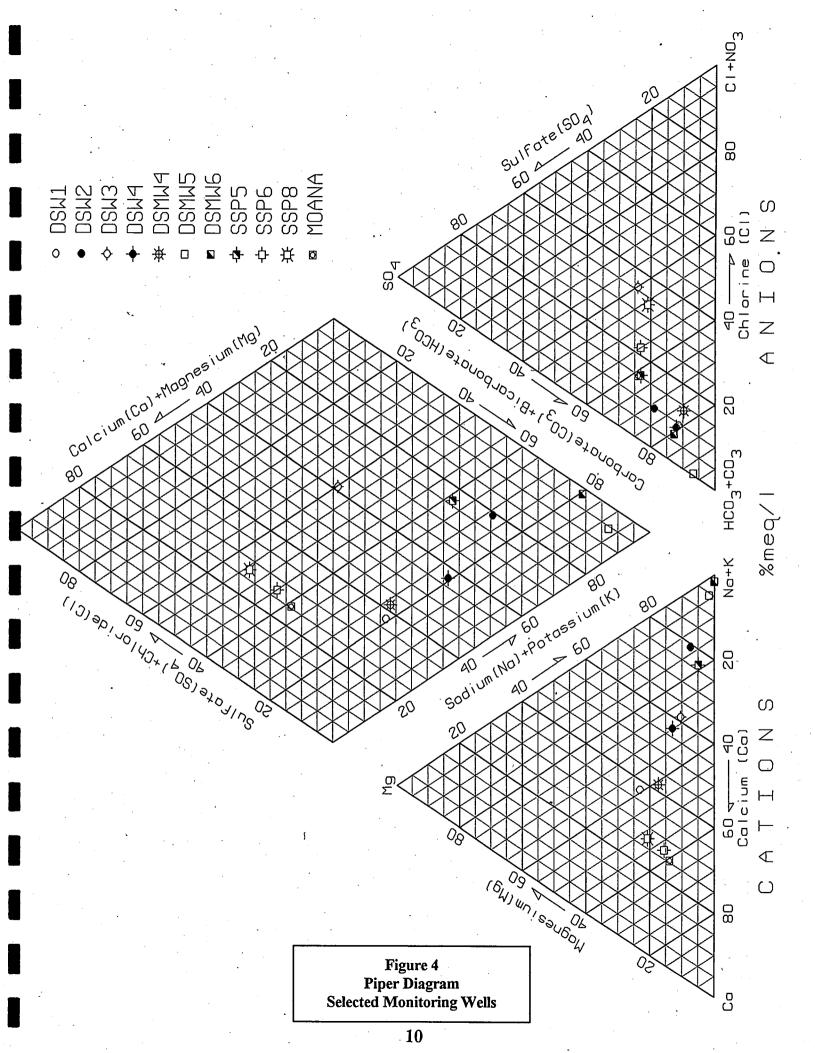
Table 3
Water Quality Summary

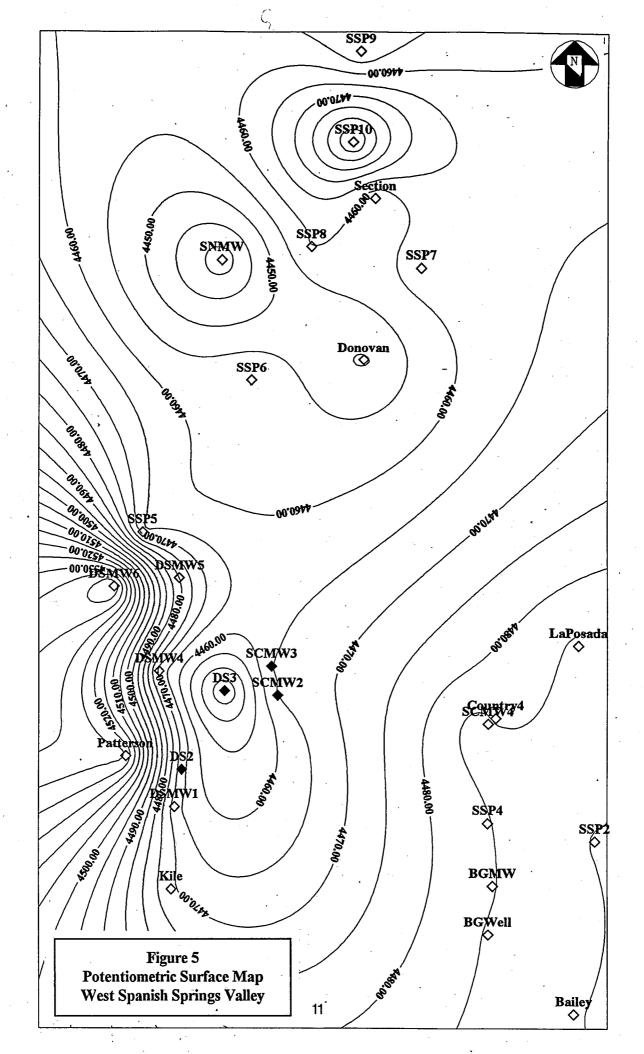
Values in mg/L

Figure 4 is a Piper diagram used to categorize the water analyses collected from the new monitoring wells and selected nearby wells. The diagram shows DSMW5 & 6 are considered to be in a aquifer containing potassium-bicarbonate waters. Bicarbonate geothermal waters can be generally associated with geothermal waters that have migrated some distance from a thermal fracture flow source and mixed with groundwater(Nicholson, 1993). Nicholson also states that higher ratios of sodium(Na) to potassium(K) are indicative of lateral flow, near surface reactions. A shallow, moderately warm, geothermal setting that is located close to a fracture zone could be applied to the area where the new monitoring wells are constructed.

The general trend of monitoring well water classification in Figure 4 indicates water quality is changing as wells transgress across the valley to the northwest. The linear anion trend from Na+K to Ca for the wells plotted probably reflect ground water percolation through different lithologic units, such as andesite sand versus granitic sand. The northeastern Spanish Springs Valley area could provide a target location for production well drilling or investigation of existing agricultural wells (Donovan Well, Figure 5) for potential purchase and use.

Figure 5 is a potentiometric surface map in feet above sea level for the Spanish Springs Valley that was generated using March, 1997 static water level measurements from 27 wells. The map shows a general flow from high elevation in the south and southwest to lower elevation in the north and northeast valley area. A steep gradient develops between DSMW5 and 6 and continues in a stretched "3" shape by DS4 and continues south to DS1. The steep contour levels suggest a structural uplift caused by faulting. The skewed "3" shape also suggests that a small depression or graben, with uplifted flanks to the north and south may enclose DS4. This is a limited interpretation based on interpolation without any static water level data or drilling information upgradient or west-southwest from DS4. Figure 5 may identify a geologic structure that isolates DS4 from poorer quality formation water observed in monitoring wells to the north and northeast. A faulted basin





could alter groundwater flow paths and provide a ground water barrier which isolates DS4 from geothermal influence. Conversely, faulting could act as a groundwater barrier in one direction while providing a mechanism for geothermal fluid transport from a larger geologic structure into another area.

#### **Conclusions**

Production wells can be constructed at either DSMW5 or DSMW6 if the arsenic concentration in the wells can be reduced by on site treatment. Elevated formation water temperature may further restrict the value of production well construction if mixing higher temperature groundwater in the existing Desert Springs Water System is considered undesirable by the WCUSD. Production well construction may be viable in the future as service areas expand since the wells have high potential well yield and low nitrate concentrations when compared to existing wells in the area. Recommendations for production well construction are found in Table 4.

Well	Cased Depth Feet	Diameter Inch	Blank Interval Feet	Screened Interval Feet	Seal Depth Feet	Screen Size Slot#
DSMW5	660	12	460	200	130	.50
DSMW6	620	12	360	260	100	80

Table 4
Production Well Recommendations

At the time of monitoring well completion, the potential for a long term agreement between Westpac Utilities and the County for wholesale water purchase and delivery to Spanish Springs Valley is viable and being actively pursued by both entities. Staff does not advocate production well construction because of the high arsenic content in the aquifer formations. Production well construction can always be reconsidered in the future when a wholesale agreement reaches completion or if water treatment technology has progressed to where arsenic removal is economical and applicable to municipal water wells. If production well construction becomes an option, the DSMW6 site is the preferred choice based upon water quality and upgradient location from existing development.

Bell, J.W., and Bonham, H.F., 1987, Vista Quadrangle (7.5 minute) Geologic Map, Nevada Bureau of Mines and Geology.

Bonham, H.F., 1969, Geology and mineral deposits of Washoe and Story Counties, Nevada, Nevada Bureau of Mines and Geology, Bulletin 70, p 51.

Fetter, C. W., 1988, Applied Hydrogeology, Merrill Publishing Co. pp 355-356.

Garside, Larry J. and Schilling, John H., Thermal Waters of Nevada, Nevada Bureau of Mines and Geology, Bulletin 91, pp 66, 134 and 138.

Klein, Cornelis, Hurlbut, Cornelius, Manual of Mineralogy, 20th Edition, John Wiley & Sons pp 480-485.

Nicholson, 1993, Geothermal Fluids, pp 19-23, 46.

## APPENDIX

DESERT SPRINGS MONITORING WELLS 5 & 6 BID RESULTS SEPTEMBER 11, 1996

				Engineers Estimate	ate	Welsco Corporation	ion	Layne Christensen Co.	en Co.
ITEM		Quantity	Units	Price	Total	Price	Total	Price	Total
-	Mobilization-Demobilization	7	Each	3000.00	6000.00	1250.00	2500.00	3200.00	6400.00
7	Drill 6 inch Borehole	1200	L. F.	18.00	21600.00	20.00	24000.00	20.00	24000.00
3	Water Quality Samples	16	Each	250.00	4000.00	425.00	6800.00	100.00	1600.00
4	Geophysical Logs	2	Each	2100.00	4200.00	3100.00	6200.00	2300.00	4600.00
	2 Inch Blank Steel Pipe	800	L. F.	7.00	5600.00	4.75	3800.00	11.00	8800.00
9	2 Inch Slotted Steel Pipe	200	L.F.	10.00	5000.00	5.95	2975.00	17.00	8500.00
7	Gravel Pack	∞	Cu. Yds	200,00	1600.00	195.00	1560.00	581.00	4648.00
<b>∞</b>	Grout Sanitary Seal	200	Feet	15.00	3000.00	. 10.00	2000.00	4.00	800.00
6	Air Development	32	Hour	250.00	8000.00	225.00	7200.00	200.00	6400.00
10	Standby	10	Hour	200.00	2000.00	135.00	1350.00	170.00	1700.00
11	Protective Well Cap	2	Each	750.00	1500.00	250.00	500.00	300.00	600.00
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## DSMW-5

#### STATE OF NEVADA

### DIVISION OF WATER RESOURCES

### WELL DRILLER'S REPORT

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PERMIT NO. M/0-1067 Issued by Water Rese	ources	N/	A Parcel No.				N/A Subdivision Name		
3. WORK PERFORM			4.	<u></u> [	DRODOGER		<del></del>		
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	Other				l/Industrial 🏅	Monitor	☐ Stock ☐ A	ir Doth	
6. LITHOL	OGIC LO	G			8.	WI	ELL CONSTRUCT	ION	
Material	Water Strata	From	То	Thick- ness	Depth Dril		reet Depth	Cased	570 Feet
SAND - GRAVEL		0	40	40	]		DIAMETER (BIT	•	
SAND - GRAVEL		40	220	180		2-1/4 Incl	hes 0 Feet	то 20	Feet
SAND - KIFE "	<u> </u>	220	225	5	╣	6-1/4 Incl	hes 20 Feet	· 690	Feet
GRAVEL - START CLAYS CLAYS - GRAY		225	405	180	-	Incl	hesFeet	·····	Feet
SAND		405	412	7		c	ASING SCHEDUL	Æ	
CLAYS - SAND STRINGERS	3	412	560	148	Size O.D. (Inches)	Weight/Ft. (Pounds)	Wall Thickness (Inches)	From (Feet)	To (Feet)
SAND GRAVELS		560	640	80	8-3/4	28.55	.312 .	0	20
CLAYS - KIFE SAND		640	680	40	2.376	5.02	.210	+2	· 460 ·
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				·	From	680	feet to 1	05	feet
		-			9.		WATER LEVEL		<del> </del>
					Static water	level 42	2 ;	feet below	v land surface
					Artesian flo	YY	/A G	.P.MN/A	P.S.I.
					Water temp	erature85	°F Quality	GOOD	
·					10.	DRILI	LER'S CERTIFICA	TION	
Date started FEBRUARY	*************	*************	************	19	This well w	as drilled und	ler my supervision a	nd the report	t is true to the
Date completed FEBRERY	10, 1	997	·····,	19	1	U	LORATORY DRII	LLING	,
7. WELL T	EST DATA	<u> </u>			l Name		Contractor		
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G.P.M. Greet 1	aw Down Below Static)		Time (Hours	s)		SALT <b>AA</b> KI	CONTRACTOR CONTRACTOR	8410 <b>4</b>	
45						tractor's licen the State Cor	se number ntractor's Board	***************************************	0021976
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					Date	EBRUARY	10, 1997		***************************************
					·			_	

WHITE—DIVISION OF WATER RESOURCES CANARY—CLIENT'S COPY PINK—WELL DRILLER'S COPY

#### STATE OF NEVADA

#### DIVISION OF WATER RESOURCES

# PRINT OR TYPE ONLY

### WELL DRILLER'S REPORT

OFFICE USE O	NLY
Log No	***************************************
Permit No.	
Basin	

DO NOT WRIT	TE ON BACK		Ple	ase comp	lete this f	orm in its ent	tirety in	7.12		
ng grander (nga kanalang ang ang ang ang ang ang ang ang ang		•				4.170 and NA		NOTICE OF	INTENT N	26240
1. OWNER	WASH	DE COUNTY	***************************************	***************************************		ADDRESS	AT WELL L	OCATION	•	•
MALING ADD	VT:00	·· <i>·</i> ·································	.y		I	SEWNTOL	r orktings	VALLEY .	·	***************************************
2 Î OCATION	NE V	NEVADA	0.9.2 <u>2.</u>						***************	***************************************
2. LOCATION	M/0-106	1/4 Se 7	c ı	NT / A		(N)S R	.υE	WASHOE	***************************************	County
PERMIT NO	Issued by Water	Resources	<u></u>	Parcel No.			•••••	Subdivision Name	)	***************************************
3	WORK PERF	ORMED		4.		PROPOSED	USE	5.	WELL 1	YPE
New Well	Replace	Recond	ition		Domestic	• • • •	Irrigation	☐ Test ☐	Cable $\square$ Re	otary 🔀 RVC
☐ Deepen	☐ Abandon			<u>-                                       </u>	Municipal	/Industrial X	Monitor	☐ Stock ☐	Air 🗆 O	ther
6	LIT	HOLOGIC LO	G			8.		ELL CONSTRU		
Ma	terial	Water Strata	From	То	Thick- ness	Depth Dri	led620			Feet
SAND GRAVE	L		0	40	40	]	HOLE	DIAMETER (From	BIT SIZE) To	
SAND - CLA			40	60	20		2-1/4 Incl	nes0_F		
SAND - GRA			60_	70	10	<u> </u>	6-1/4 Incl	nes 20 F	eet620	
BROWN CLAY		STATI		90	20				eet	
SANDY CLAY			90	100	10		C	ASING SCHED		
_CLAYS - SO			100_	130_	30	Size O.D.	Weight/Ft. (Pounds)	Wall Thickness		То
GREY CLAY			130_	226	96	(Inches)	(Pounds)	(Inches)	(Feet)	(Feet)
CLAY -SAND			226	250_	24	8-3/4		.312		20
GRAY CLAY SAND GRAVE			250_	290_	40	2.376		210	+2	271
GRAY CLAY			290	300_	10	<u> </u>	L	<u> </u>		
SAND - GRA			300 330	330 340	30	Perforation	s: erforation	SLOT	•	
GRAY CLAY			340_	350	10 10	Size pe	rforation	3/32	******************************	1
SAND GRAVE			350_	400	50	From2	7.1	feet to	523	feet
SAND GRAVE		CLAYS	400	450°	50	From		feet tofeet to	***************************************	feet
SAND GRAVE			450	520	20	From	***************************************	feet to	••••••	feet
SAND - CLA		•	520	620	100	From	*************************	feet to	***************************************	feet
	· .						al: 🛛 Yes		Seal '	
									[ <del>]</del>	Neat Cement
							Method: 🛛			Cement Grout
								Poured		Concrete Grout
<del></del>						Gravel Paci	ked: □XYe	es 🗆 No		•
.,	•					From		feet to	130	feet
•	• :			<u> </u>		9.		WATER LEVE		
· · · · · · · · · · · · · · · · · · ·			<u> </u>			11	r level	76		ow land surface
•								N/A		
-							erature9		yGO0	
						10.	ו זומת	LER'S CERTIFIC	<del></del>	
	7777		الع			11		ler my supervisio		ort is true to the
Date started						best of my	knowledge.	or my supervisio	ni and the rept	ore is true to the
Date completed			<del></del>		, 199.7.	Name	LANG EXP	ORATORY DI	RILLING	
<u>7.                                      </u>	WEL	L TEST DAT	A					Contracto	or	
TEST ME	ETHOD: □	Bailer	Pump	🖫 Air Li	ft -	Address	2286 WEST	Contract		······································
	G.P.M.	Draw Down Feet Below Static	,	Time (Hou	rs)		SALT AAKI	E CITY, UTA	AH, 84104	
	30						tractor's licen		*	0021076
-		· ·			,	1		tractor's Board		0021976
·				<u> </u>		Division	ner's incense r of Water Reso	number issued by ources, the on-site	ne e driller	1410
			at .			•		7	- 1 /	·
					·	Signed	JOHN VIER By driller po	RGUTS Corning actual dril	My /Ce	natura
•	- :	<del></del>		-:		Date		FEBRUARY		• ,

### NEVADA STATE HEALTH LABORATORY

DSMW NEVADA DIVISION OF HEALTH

L Virginia Street Reno yada 89503

131399

### VATER CHEMISTRY ANALY

Attn: Fees may apply to some types of sampl

TYPE OF ANALYSIS:

Check here for ROUTINE DOMESTIC ANAI Circle the constituents needed for PARTIAL ANA All of the information below must be filled in . or the analysis will not be performed.

State NEVADA	WASHOE 34
Township Range Range	20E Section 34
General Location SPANISH	SPRINGSection 34 TON OF ALENA WAY CATETY
Source Address.	TON OF ALENA WAY TOATETE

SAMPLING INSTRUCTIONS
-----------------------

The sample submitted must be representative of the source. Spring and surface water samples should be as free of dirt and debris as possible. Wells should be pumped thoroughly before sampling, changing the water in the casing at least three times. Product water from filters should be sampled after running for about ten (10) minutes.

Sampled by DAN DIZALAN 1/20/97 WASHOE CCUNTY

REPORT	TO.		•	
REFURI	TO:	TUANICE	MICUD	
Name	ED.	EVANS	WCUD	

P.O. BOX 11130

EASON FOR ANALISIS	: USE OF WATER:
Loan	Domestic drinking water

☐ Geothermal Personal health reasons ☐ Purchase of the property  $\square$  Industrial or mining

☐ Rental or sale of property Subdivision approval

☐ Irrigation Other MICHITI RING WELL DSMW5 Initials.

#### SOURCE OF WATER:

Filter  Yes  No	Т
Public ☐ Yes 🗡 No	N
Spring X Depth 670 ft.	S
Wellft.	C
HotCold	C

MONITORING WILL Jame Casing diameter \_\_\_\_\_in.

asing depth.....ft. IN USE ☐ Yes D No

The results below are representative only of the sample submitted to this laboratory.

0.1330	341	0.69 FO	r <sub>2</sub> Į arorat	oba Are one	9 <sup>Y</sup> . 7 3	13 131	399	PRINT OTH CONSTITUI	IER DESIRED ENTS BELOW
Constituent	ppm	Constituent	ppm	Constituent	ppm	Constituent	s.u.	Constituent	ppm
T.D.S. @	337	Chloride	14	Iron	1.91	Color	> 70	Cd	<0.001
Hardness	14	Nitrate -N	0.1	Manganese	0.05	Turbidity	65.0	Cr 🦡	10.005
Calcium	4	Alkalinity	146	Copper	0.02	pН	8.65	Pb	<0.005
Magnesium	1	Bicarbonate	144	Zinc	0.00	EC	491	На	100005
Sodium	108	Carbonate	17	Barium	0.02	SI@20C	-0.14	Se ·	<000
Potassium	1	Fluoride	2.12	Boron	0.4			Aq	40,005
Sulfate	69	Arsenic	0.117	Silica	52			يتكه كرمين	Contraction of the second
				GACSS ALPHA	<3 P.4	PADIUM		APK	
			•	GRUSS BETA	< 3 P/e	MEAS	<0.1	P.C.	A STREET H
-	./	Δ.		2001					- Train Gray

/ 100	
133	
//	
Sec	
	1/3,

om = parts per million, milligrams per liter U. = Standard Units

9

O-1561 (Rev. 4-92)

IN TRIPLICATE.

### NEVADA STATE HEALTH LABORATORY

NEVADA DIVISION OF HEALTH

1660 N. Virginia Street Reno, Nevada 89503

(702) 688-1335 ·

DSMW6

O-1561 (Rev. 4-92)

All of the information below must be filled in W... TER CHEMISTRY ANALYSIS: or the analysis will not be performed. Attn: Fees may apply to some types of samples. County WASHOE TYPE OF ANALYSIS: Township 21N Range 20E Check here for ROUTINE DOMESTIC ANALYSIS.

Circle the constituents needed for PARTIAL ANALYSIS. General Location SPANISH SPRINGS VALLEY

Aller.		•			Source Ad	aress	EL WEST OF	DEAN DRIVE			
SAMPLING INSTRUCTIONS:  The sample submitted must be representative of the source. Spring and surface water samples should be as free of dirt and debris as possible. Wells should be pumped thoroughly before sampling, changing the water in the casing at least three times. Product water from filters should be sampled after running for about ten (10) minutes.  Sampled by ED EVANS - WCUD Date 1/15/97  Owner WASHOE COUNTY Phone 856-7300  Address P.O. Box 11130  City RENO State NEVADA  REPORT TO:  Name ED EVANS - WCUD  Address P.O. Box 11130  City RENO  State NY					Domestic drinking water     Loan   Domestic drinking water     Personal health reasons   Geothermal     Purchase of the property   Industrial or mining     Rental or sale of property   Industrial or mining     Subdivision approval   Other Patential Municipal     Other Patential Municipal   Initials     WELL LOCATION     SOURCE OF WATER:     Filter   Yes   No   Name   DSYMWL6     Spring   Surface     Well   Depth   620   ft   Casing diameter   2   in     Hot   Cold   Casing depth   525   ft						
<u> </u>	The	results below	gra rantasa	ntative only	of the sample	a submitted t	a this labora	4000	· · · · · · · · · · · · · · · · · · ·		
\(\). \(\frac{1\(\text{x}\)}{\tag{x}}		<del></del>	<del></del>	<del></del>		e submitted to	o this labora	PRINT OTHE	D DECIDED		
Constituent 993	1,9,3		R LABORAT 16.1 <sub>ppm</sub>	ORY USE ONI		O9 <sub>Constitu</sub> 1,31	347	CONSTITUEN	ITS BELOW		
T.D.S. @ 103° C.	199	Chloride	7	Iron	O.13	Color	15	Constituent	<0.00		
Hardness	3	Nitrate - N	0.0	Manganese	0.00	Turbidity	3.5	Cr	10,005		
Calcium	. 1	Alkalinity	118	Copper	0.00	рН	8.90	Se	10:00		
Magnesium	0	Bicarbonate	95	Zinc	0.00	EC ·	307	Pb	10.005		
Sodium	72	Carbonate	24	Barium	0.01	SI@20C	-0.56	Hg	10.0005		
Potassium	0	Fluoride	0.93	Boron	0.1		<u> </u>	Ag	10.005		
Sulfate	18	Arsenic	0.060	Silica	34			<u> </u>	759		
	:			GROSS ALPHA	K3 Pye	RADIUM 226		APR 0 3	1997		
				GILOSS BETA	<3 P/2	MBAS	(0.1	BURGAU OF			
} Fee	•••••		Remarks	Use PO # 1	58 <b>853</b>	Eg (-)	107	PRUIZOTION Carsen	City K		
Collected by			NEVAC	AL QUALITY MEE A DRINKING WATI	TS THE STATE OF ER STANDARDS	94) N	, , , , , , , , , , , , , , , , , , , ,	2/4/			
st2nd		3rd	PA	H Stand RSENIC	dard PA Stany	inge-6 dard (	,5-8,5 7,05	s.u. g	gn		
pm = parts per million .U = Standard Units	, milligrams p	er liter		·				¥.			



#### Laboratory **Analysis Report**

Sierra

**Environmental** Monitoring, Inc.

.: 1/23/97 Client : WAS-314

Taken by: CLIENT-E. EVANS

Page:

Report : 18649 PO# : 160395

WASHOE COUNTY UTILITY DIV.

ED EVANS

P.O. BOX 11130 **RENO NV 89520** 

	 			 	raye. I
Sample	Collected Date Time	NITRATE-N MG/L	ARSENIC ICP-MS MG/L		
MW5 - 180 MW5 - 410 MW5 - 580 MW5 - 680	1/16/97 11:45 1/17/97 9:00 1/17/97 14:45 1/17/97 18:30	2.1N 4.2N 2.4N <1N *	0.085 0.098 0.11 0.18		

Approved By:

This report is applicable only to the sample received by the laboratory. The liability of the laboratory is limited to the amount paid this report. This report is for the exclusive use of the client to whom it is addressed and upon the condition that the client summes all liability for the further distribution of the report or its contents.

### Laboratory Analysis Report

WASHOE COUNTY UTILITY DIV.

ED EVANS

P.O. BOX 11130 RENO NV 89520 Sierra Environmental Monitoring, Inc.

Date : 1/17/97 Client : WAS-314

Taken by: CLIENT-E. EVANS

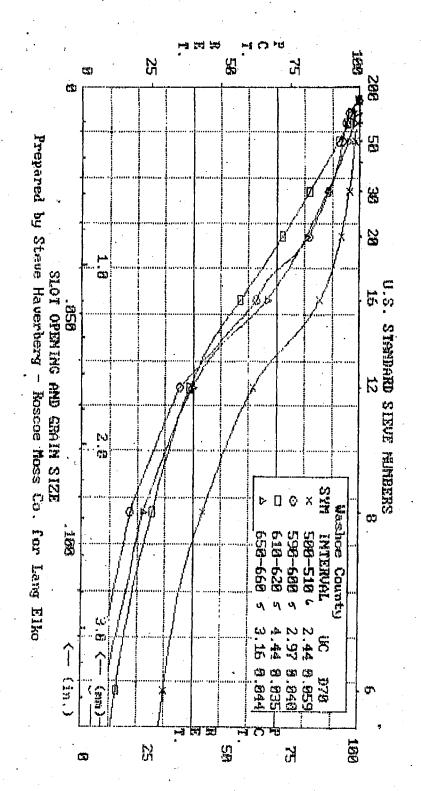
Report : 18593 PO# : 160395

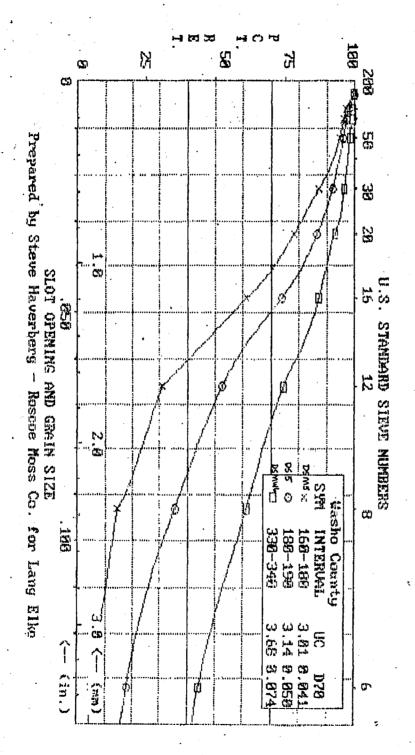
Page: 1

Sample	Col! Date	ected Time	NITRATE-N MG/L	ARSENIC ICP-MS MG/L	•		rage. 1
MW6-200 MW6-260 MW6-340 MW6-400 MW6-460 MW6-560 MW6-610	1/10/97 1/10/97 1/10/97 1/11/97 1/11/97 1/11/97	7 15:30 7 17:45 7 9:30 7 11:30 7 13:30 7 16:15	0.3N <0.1N <0.1N <0.1N <0.1N <0.1N	0.088 0.12 0.068 0.061 0.065 0.076		•	

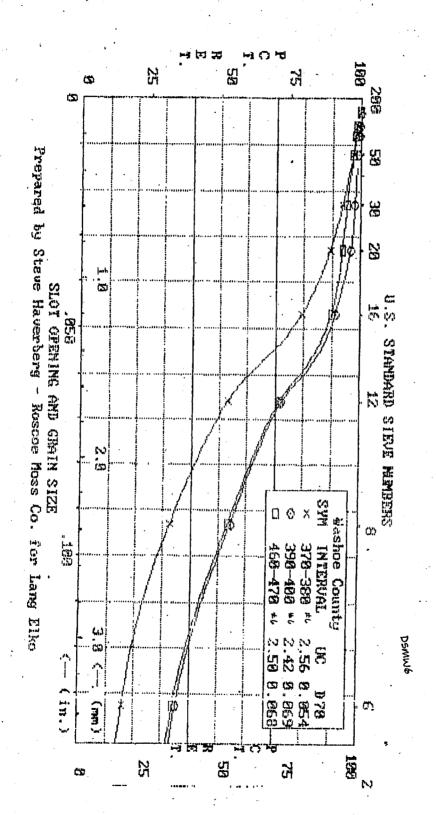
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CLIENT: Lang Elko



CLIENT: Lang Elko PROJECT: Washo County

#### SAMPLE

		160-	LBO	180-2	190	330-3	340
Mesh	SIZE						
NO.	(IN)	CUWT	<b>%RET</b>	CUWT	<b>RET</b>	CUWT	<b>ERET</b>
3	. 263	•		Y*			
1/4	.250	*	,		٠.		•
4 -	.187	5.0	2	21.0		81.0	30
6	.132	$\cdot 13.0$	5	50.0	18:	L21.0	44
8	.093	39.0	15	99.0	36:	168.0	61
12	.066	83.0	31:	146.0	532	204.0	74
16	047	163.0	61	205.0	742	239.0	87
20	.033	209.0	78	241.0	872	255.0	93
30	.023	233.0	87	256.0	922	264.0	96
40	.016						
50	-012	253.0	95	267.0	962	270.0	99
70	.008	257.0	96	270.0	97	272.0	99
100	.006	259.0	97	272.0	983	272.2	99
PAN	.003	267.0	100	278.0	100	274.0	100

#### TRET SIZE TRET SIZE TRET SIZE 30 0.068 30 0.102 30 0.185 40 0.060 40 0.086 40 0,147 50 0.054 50 0.069 50 0.116 60 0.048 60 0.058 60 0.096 70 0.041 70 0.050 70 0.074 80 0.031 80 0.041 80 0.059 90 0.020 90 0.027 90 0.040 UC 3.01 UC 3.14 UC 3.68

Analysis by Stave Haverberg - Roscoe Moss Co.

CLIENT: Lang Elko

PROJECT: Washoe County

#### SAMPLE

					~~~~~~~			
•	. * *	370-3	380	390-	400	460~	470	
mesh	SIZE							
NO.	(NI)	CUWT	<b>tret</b>	CUWT	FRET	CUWT	<b>TRET</b>	
3	. 263							
1/4	. 250					•		
4	.187	18.0	7	57.0	21	54.0	19	
6	.132	44.0	16	97.0	35	95.0	34	
8	.093	90.0	33:	149.0	54:	148.0	53	
12	.066	146.0	533	198.0	72:	198.0	71	
16	.047	219.0	792	250.0	912	249.0	90	
20	.033	247.0	892	265.0	972	260.0	94	
. 30	.023	259.0	942	269.0	982	264.0	95	
40	.016		•					
50	.012	269.0	972	272.0	992	270.0	97	
70	.008	272.0	99	273.0	1002	272.0	98	
100	.006	273.0	992	273.1	1002	273.0	99	
PAN	.003	276.0	1002	274.0	1002	277.0	100	

#### TRET SIZE TRET SIZE TRET SIZE

1 30 0.147
9 40 0.117
0 50 0.099
4 60 0.082
9 70 0.068
0 80 0.059
9 90 0.047
֡

UC 2.56 UC 2.42 UC 2.50

Analysis by Steve Haverberg - Roscoe Moss Co.

CLIENT: Lang Elko PROJECT: Washoe County

		SAMP	Le .						
Vacu		500-510		590-600		610-620		650-660	
MESH NO.	SIZE (IN)	CUWT	*RET	CUWT	ARET	CUWT	RET	CUWT	TRET
3/4 2600000 57000 PAN	.2630 .21872 .13936 .0047 .00128 .00063	58.0 82.0 120.0 169.0 235.0 257.0 271.0 273.0 274.0	99 99 100	1.0 11.0 43.0 87.0 156.0 220.0 233.0 233.0		12.0 30.0 60.0 92.0 135.0 171.0 194.0 219.0 227.0 2230.0		8.0 21.0 54.0 98.0 64.0 18.0 237.0 242.0	39 22 40 66 81 88 96 99 100
	•	\$RET	SIZE	*RET	SIZE	*RET	SIZE	<b>tret</b>	SIZE
		30 40 50 60 70 80	0.131 0.099 0.082 0.068 0.059 0.052	30 40 50 60 70 80 90	0.074 0.063 0.056 0.049 0.040 0.034	30 (40 (50 (60 (60 (60 (60 (60 (60 (60 (60 (60 (6	0.083 0.064 0.053 0.044 0.035 0.025	30 40 50 60 70 80 90	0.080 0.066 0.057 0.051 0.044 0.034
•	•	UC	2.44	UC	2.97	UC	4.44	บต	3.16

Analysis by Steve Haverberg - Roscoe Moss Co.